

## V. Simplified bare pixels sensitivity calculations compared to a similar work by Desert

In "The case for a bolometric millimetre camera at the IRAM 30m telescope", Astro-ph 29 Jan 1999 and IRAM Newsletter Jan 1999, Désert & Benoit presented an estimation of bolometer performances for the 30m. Using the updated revision by Desert (2008), these performances are calculated again below and compared with a simplified version of my estimations to verify (1) the consistency of my procedure, (2) that with some approximations only few simple calculations are necessary, and (3) illustrate the effect of some variations in the input parameters.

<u>Input parameters and hypothesis:</u>		
<b>Desert :</b>	Telescope area: $A = 707 \text{ m}^2$	<b>Me:</b>
2 wavelengths $ii := 0..1$		
$\lambda_D := \begin{pmatrix} 2.1 \\ 1.2 \end{pmatrix} \text{ mm}$	$v_D := \frac{c}{\lambda_D}$ $v_D = \begin{pmatrix} 143 \\ 250 \end{pmatrix} \text{ GHz}$	$\lambda_{ii+1} = \begin{pmatrix} 2.05 \\ 1.25 \end{pmatrix} \text{ mm}$ $v_{ii+1} = \begin{pmatrix} 146 \\ 240 \end{pmatrix} \text{ GHz}$
$\frac{\delta v}{v} := 0.30$ $v_{Dm} := v_D \cdot 0.85$ $v_{DM} := v_D \cdot 1.15$		$\frac{\delta \lambda}{\lambda} = \frac{2 v_{ii+1} \cdot w_{ii+1}}{(v^2 - w^2)_{ii+1}} = \begin{pmatrix} 0.28 \\ 0.39 \end{pmatrix}$
$\delta v_D := v_{DM} - v_{Dm}$	$\delta v_D = \begin{pmatrix} 43 \\ 75 \end{pmatrix} \text{ GHz}$	$2 w_{ii+1} = \begin{pmatrix} 40 \\ 90 \end{pmatrix} \text{ GHz}$

Writing the pixel size  $uF\lambda$  (see II.), the throughput  $S\Omega = (\pi D^2/4) \cdot ((\pi/4) \cdot (u \cdot \lambda/D)^2) = (\pi/4) \cdot u^2 \cdot \lambda^2$

Desert takes a pixel sampling a FWHM beam, (he uses the true factor 1.03, I approximate it with 1).

I take  $0.5 F\lambda$  for both bands, but with a 5% gap between pixels:

$u_D := \begin{pmatrix} 0.5 \\ 0.5 \end{pmatrix}$ $S\Omega_{D_{ii}} := \left( \frac{\pi}{4} \right)^2 \cdot \left( 1.03 \cdot u_{D_{ii}} \cdot \lambda_{D_{ii}} \right)^2$	D vs me:	$u_{me} := 0.95 \cdot 0.5$ $u_{me} = 0.475$ $S\Omega_{me_{ii}} := \frac{\pi}{4} \cdot (0.475 \cdot \lambda_{ii+1})^2$
$S\Omega_D = \begin{pmatrix} 0.72 \\ 0.24 \end{pmatrix} \text{ mm}^2 \text{ sr}$ = $E_p = E_{eff}$ in Desert's sheet	$\frac{\pi}{4} \cdot \left( \frac{1.03}{0.95} \right)^2 = 0.92$	$S\Omega_{me} = \begin{pmatrix} 0.74 \\ 0.28 \end{pmatrix} \text{ mm}^2 \text{ sr}$

$$T_{aD} := 250\text{K} \quad T_{tD} := 280\text{K} \quad T_{supD} := 280\text{K} \quad T_{atm} = 270\text{K} \quad T_{tel} = 280\text{K} \quad T_{f_{me}} := 77\text{K}$$

From my calculations in II.2., the dominant background is due to atmosphere and telescope, and in a lesser extent the 77K stage. In Desert the filter transmission is low compared to mine (see below), which means a higher emissivity thus a higher contribution, but he includes the filters in a global term  $P_{sup}$  including also mirrors, window and lens; at 280K with a 5% emissivity.

### Transmission factors:

#### 1) atmosphere

$\tau_{D1mm} := 0.35 \Rightarrow \text{ATM gives:}$	$\tau_{D2mm} := 0.13$	$\tau(v_{ii+1}, 0) = \begin{pmatrix} 0.07 \\ 0.13 \end{pmatrix}$	$\tau(v_{ii+1}, 1) = \begin{pmatrix} 0.29 \\ 0.69 \end{pmatrix}$
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Desert atmosphere is not great (~4mm wv), but between my 2 extreme choices

$ea_D := 1 - \exp \left[ - \begin{pmatrix} \tau_{D2mm} \\ \tau_{D1mm} \end{pmatrix} \right]$	$ea_D = \begin{pmatrix} 0.12 \\ 0.30 \end{pmatrix}$	$ea_{me_{ii,v}} := ea(v_{ii+1}, v)$	$ea_{me} = \begin{pmatrix} 0.07 & 0.25 \\ 0.12 & 0.50 \end{pmatrix}$
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Remark: though  $T_{\text{atm}} - T_{\text{D}} = 20\text{K}$ , for identical contents of water vapor my  $\tau_{\text{me}}$  is few % <  $\tau_{\text{D}}$  because Desert's  $\tau$  are at Zenith whereas mine are corrected for 50 degree elevation.

$$\epsilon_{\text{D}} := 0.1$$

2) telescope emissivity

$$\epsilon_{\text{t}} = 0.11$$

3) filters + 77K lens

I choose  $n_{\text{fb}} = 7$  filters stages plus the band pass filter plus 1 lens, each with a transmission  $t_{\text{f}} = 95\%$  but only  $n_{\text{f77}} = 3$  on the 77K stage while the others are at colder stages.

Desert assumes a warm lens, I find [thesis]  $e(2\text{cm}) = 5\%$ , but he took  $e(5\text{cm}) = 15\%$ , (my  $t_{\text{fD}} = \text{his } t_{\text{filt}} \cdot t_{\text{len}}$ )

$$t_{\text{fme}} := t_{\text{f}}^{n_{\text{fb}}+1} \quad t_{\text{fme}} = 0.66$$

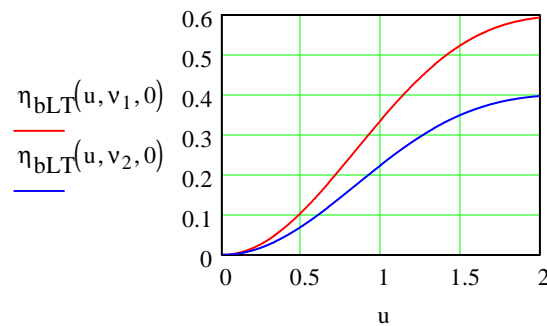
$$t_{\text{fD}} := 0.15 \cdot 0.85 \quad t_{\text{fD}} = 0.13 \quad \epsilon_{\text{fD}} := 1 - t_{\text{fD}} \quad \epsilon_{\text{fD}} = 0.87 \quad \epsilon_{\text{fme}} := 1 - t_{\text{f}}^{n_{\text{f77}}} \quad \epsilon_{\text{fme}} = 0.14$$

0.15 vs 0.66 ==> Desert filters are really bad compared to Cardiff's specifications !

If I would use filters as bad as Desert's, I would have to choose  $T_{\text{f}} \ll 10\text{K}$  to avoid  $P_{\text{f}}$  dominates the background ! Desert avoid the problem introducing an artificial  $\epsilon_{\text{sup}} = 5\%$  ; suspicious (see below) !

4) efficiency linked to the diffraction pattern

The figure opposite shows the integral of the diffraction pattern up to the pixel size ( $u$ ) in unit of  $F\lambda$  ( $\Rightarrow \eta_{\text{bLT}} = \text{pixel efficiency}$ ). The red line is for the 2mm band and the blue line for the 1mm band.  $u=0.5$  is required for Nyquist sampling and gives  $\eta_{\text{pix}}$ .  $u=1$  is for beam sampling (= FWHM).  $u=2$  is the full beam (1<sup>st</sup> dark ring) and gives  $\eta_{\text{Beff}}$ .



The only efficiency related to the diffraction pattern in Desert's Excel sheet is his main lobe efficiency:

$$\text{EffLP} := \begin{pmatrix} 0.50 \\ 0.25 \end{pmatrix}$$

$$\text{pixel: } \eta_{\text{pixme}_{ii}} := \eta_{\text{bLT}}(r_{\text{s}} \cdot u_{\text{me}}, v_{ii+1}, 0)$$

$$\text{FWHM: } \eta_{\text{HPme}_{ii}} := \eta_{\text{bLT}}(r_{\text{s}} \cdot 1 \cdot 0.95, v_{ii+1}, 0)$$

$$\text{1<sup>st</sup> ring: } \eta_{\text{Beffme}_{ii}} := \eta_{\text{bLT}}(r_{\text{s}} \cdot 2 \cdot 0.95, v_{ii+1}, 0)$$

$$\eta_{\text{pixme}} = \begin{pmatrix} 0.13 \\ 0.09 \end{pmatrix} \quad \eta_{\text{HPme}} = \begin{pmatrix} 0.38 \\ 0.26 \end{pmatrix} \quad \eta_{\text{Beffme}} = \begin{pmatrix} 0.60 \\ 0.40 \end{pmatrix}$$

Usually "main lobe" refers to the full beam ( $2F\lambda$ ), it seems this is what he means in his calculation of the power from a point source (see the factor  $\text{EffLP}/5$  below), but his calculation of the NEFD suggests he rather means FWHM efficiency ("4 pixels per beam") !

For the 2mm band  $\text{EffLP}$  is between my Half Power efficiency and beam 1<sup>st</sup> dark ring efficiency, whereas for the 1mm band  $\text{EffLP} = \eta_{\text{HPme}}$ . Does this mean that one of Desert's values is wrong ?

5) others

leakage & blockage  $t_{\text{o}} = 0.97$

Apparently no other factors for D&B

detector quantum efficiency  $\eta_{\text{d}} = 0.90$

$$\text{forward efficiency } F_{\text{eff}_{ii+1}} = \begin{pmatrix} 0.90 \\ 0.86 \end{pmatrix}$$

In his 2008 revision, Desert added calculations for the same  $\lambda$  as me, with filters closer to mine  $tf_{Dnew}=0.7$ , a revised EffLP that I cite below as  $B_{eff}$  because the values come from Beff in Greve's article "The beam pattern of the IRAM 30m telescope", and the other factors follow the same rule as his "initial case". The ratios of his **"best case" factors versus my transmission factors**:

$\lambda$ :	$S\Omega$ :	t atmo:	$B_{eff}$ :	telescope + lens filters + others (but without $F_{eff}$ ):	Global ratio without $B_{eff}$ :
2.05mm	$\frac{69}{74} = 0.93$	$\frac{0.96}{1 - 0.07} = 1.03$	$\frac{0.54}{0.60} = 0.90$		$\frac{1.03^2 \cdot 0.93}{F_{eff_{ii+1}}} = \begin{pmatrix} 1.10 \\ 1.15 \end{pmatrix}$
1.25mm	$\frac{26}{28} = 0.93$	$\frac{0.91}{1 - 0.12} = 1.03$	$\frac{0.42}{0.40} = 1.05$	$\frac{0.7 \cdot 0.85}{0.66 \cdot 0.97 \cdot 0.9} = 1.03$	

==> Desert's "best case" global transmission is comparable to mine, whereas the match with his "initial case" is really poor (global ratio D/me=0.24) because of his bad filters. Keeping the bad filters for the continuation of the comparison below will bring an interesting result.

#### 6) Global factors for atmosphere, telescope and cryostat optics

$$\begin{aligned}
 eta_D &:= ea_D \cdot (1 - et_D) \cdot tf_D & eta_{me_{ii,v}} &:= ea_{me_{ii,v}} \cdot (1 - et) \cdot tf_{me} \cdot (to \cdot \eta_d \cdot F_{eff_{ii+1}}) \\
 ett_D &:= et_D \cdot tf_D & ett_{me_{ii}} &:= et \cdot tf_{me} \cdot (to \cdot \eta_d \cdot F_{eff_{ii+1}}) \\
 \text{Desert has no direct contribution of filters, but an artificial } e=5\% \text{ warm optics contribution:} & & etf_{me} &:= ef_{me} \cdot tf^{nfb-nf77} \\
 etsup_D &:= tf_D \cdot 0.05 & etsup_D &= 0.64 \% \\
 tsky_D &:= (1 - ea_D) \cdot (1 - et_D) \cdot tf_D & tsky_{me_{ii,v}} &:= (1 - ea_{me_{ii,v}}) \cdot (1 - et) \cdot tf_{me} \cdot (to \cdot \eta_d \cdot F_{eff_{ii+1}}) \\
 eta_D &= \begin{pmatrix} 1.4 \\ 3.4 \end{pmatrix} \% & ett_D &= 1.3 \% \\
 & & etsup_D &= 0.6 \% \\
 tsky_D &= \begin{pmatrix} 10 \\ 8 \end{pmatrix} \% & eta_{me} &= \begin{pmatrix} 3.3 & 11.9 \\ 5.3 & 22.3 \end{pmatrix} \% \\
 & & ett_{me} &= \begin{pmatrix} 5.5 \\ 5.3 \end{pmatrix} \% \\
 & & etf_{me} &= 11.6 \% \\
 & & tsky_{me} &= \begin{pmatrix} 43 & 35 \\ 39 & 22 \end{pmatrix} \%
 \end{aligned}$$

#### Heat load from background power:

$$\text{Recall of Plank black body brightness : } Br(T, \nu) := \frac{2 \cdot h}{c^2} \cdot \frac{\nu^3}{\exp\left(\frac{h \cdot \nu}{k \cdot T}\right) - 1}$$

Assuming the product  $S\Omega(\nu) \cdot et(\nu) \cdot Br(\nu)$  is roughly linear in the bandwidth  $\delta\nu$ , its integration can be approximated with the product  $S\Omega(\nu_c) \cdot et(\nu_c) \cdot Br(\nu_c) \cdot \delta\nu$  where  $\nu_c$  is the band center, thus giving simple formulas for the power deposited on the detectors:

$$\begin{aligned}
 P_{aD_{ii}} &:= S\Omega_{D_{ii}} \cdot eta_{D_{ii}} \cdot Br(T_{aD}, \nu_{D_{ii}}) \cdot \delta\nu_{D_{ii}} & P_{ame_{ii,v}} &:= S\Omega_{me_{ii}} \cdot eta_{me_{ii,v}} \cdot Br(T_{atm}, \nu_{ii+1}) \cdot 2 \cdot w_{ii+1} \\
 P_{tD_{ii}} &:= S\Omega_{D_{ii}} \cdot ett_D \cdot Br(T_{tD}, \nu_{D_{ii}}) \cdot \delta\nu_{D_{ii}} & P_{tme_{ii}} &:= S\Omega_{me_{ii}} \cdot ett_{me_{ii}} \cdot Br(T_{tel}, \nu_{ii+1}) \cdot 2 \cdot w_{ii+1} \\
 P_{supD_{ii}} &:= S\Omega_{D_{ii}} \cdot etsup_D \cdot Br(T_{supD}, \nu_{D_{ii}}) \cdot \delta\nu_{D_{ii}} & P_{fme_{ii}} &:= S\Omega_{me_{ii}} \cdot etf_{me} \cdot Br(T_{fme}, \nu_{ii+1}) \cdot 2 \cdot w_{ii+1}
 \end{aligned}$$

$$P_{TD} := P_{aD} + P_{tD} + P_{supD}$$

$$P_{Tme_{ii,v}} := P_{ame_{ii,v}} + P_{tme_{ii}} + P_{fme_{ii}}$$

$$P_{aD} = \begin{pmatrix} 0.67 \\ 2.80 \end{pmatrix} pW \quad P_{tD} = \begin{pmatrix} 0.68 \\ 1.18 \end{pmatrix} pW \quad P_{ame} = \begin{pmatrix} 1.7 & 6.2 \\ 6.2 & 26.0 \end{pmatrix} pW \quad P_{tme} = \begin{pmatrix} 3.0 \\ 6.4 \end{pmatrix} pW$$

$$P_{supD} = \begin{pmatrix} 0.3 \\ 0.6 \end{pmatrix} pW \quad \boxed{P_{TD} = \begin{pmatrix} 1.7 \\ 4.6 \end{pmatrix} pW} \quad P_{fme} = \begin{pmatrix} 1.7 \\ 3.7 \end{pmatrix} pW \quad \boxed{P_{Tme} = \begin{pmatrix} 6.4 & 10.8 \\ 16.2 & 36.0 \end{pmatrix} pW}$$

Desert's sheet using my Thesis polynomial approximation for atmospheric transmission:

My values with the exact calculations from III.2.:

$$P_{ads} := \begin{pmatrix} 0.77 \\ 3.05 \end{pmatrix} pW \quad \text{His total: } P_{Tds} := \begin{pmatrix} 1.9 \\ 4.9 \end{pmatrix} pW \quad P_{Tm_{ii,v}} := P_{ab_{ii+1,v}} + P_{tb_{ii+1}} + P_{77b_{ii+1}}$$

$$P_{Tm} = \begin{pmatrix} 6.3 & 10.7 \\ 16.5 & 36.7 \end{pmatrix} pW$$

My results are consistent with III.2. ==> the linear approximation of the spectral power in the bandwidth is correct (and  $P_{tD}$  1% < Desert's Excel sheet 3<sup>rd</sup> order polynome approximation of Br).

- Atmosphere:  $|P_{aD} - P_{adD}| > 0$  comes from the transmission (opacity) model ; Desert uses a 3<sup>rd</sup> order polynome fit for each band (from my thesis), more precise than the global multiband fit I defined in III.1. Beside the atmosphere model, the other transmission factors contribute to the difference between Desert's sheet and  $P_{ame}$ .
- Telescope: the transmission factors explain the difference between Desert's sheet and me.
- Cryostat optics: Desert's  $P_{sup}$  using his "best case" transmission factors (0.7 for the filters) is  $\sim P_{fme}$ , though calculated with different hypothesis, mostly because his  $T_{sup} >$  to my  $T_f$  is compensated by his low "supplementary" emissivity ( $\epsilon_{sup}=5\%$ ). But using the very low transmission of his "initial case" filters (0.15) in my method gives a very big filter emissivity, thus a very strong totally dominant and unrealistic contribution of the filters to the background.

Beside these differences, our calculations are consistent with each other so far.

Remark: my optics description [77K + 4K + cold parts] seems more realistic than Desert's low transmission, low emissivity, warm supplementary component. Nevertheless my method assumes  $\epsilon + t = 1$ , hence reflection is neglected. For the mirrors reflection = transmission of the signal to the cryostat (so it's OK), but for the filters the reflection is back to the sky. Thus  $P_{fme}$  may be actually lower than my calculation, but the filters transmission shouldn't be changed, hence neither the effect on the other background sources, so I still prefer my method.

#### Typical sources power

$$\text{Extended source: } T_{RJt} := 1K \quad B_{RJt}(\lambda) := \frac{2 \cdot k \cdot T_{RJt}}{\lambda^2}$$

$$P_{rjD_{ii}} := S\Omega_{D_{ii}} \cdot \text{tsky}_{D_{ii}} \cdot B_{RJt}(\lambda_{D_{ii}}) \cdot \delta v_{D_{ii}} \quad P_{rjme_{ii,v}} := S\Omega_{me_{ii}} \cdot \text{tsky}_{me_{ii,v}} \cdot B_{RJt}(\lambda_{ii+1}) \cdot 2 \cdot w_{ii+1}$$

$$P_{rjD} = \begin{pmatrix} 19.5 \\ 27.4 \end{pmatrix} fW \quad P_{rjme} = \begin{pmatrix} 85 & 68 \\ 173 & 98 \end{pmatrix} fW \quad \text{From III.2. @ 1mmwv:}$$

$$\text{With EffLP: } \text{EffLP}_{ii} \cdot P_{rjD_{ii}} = \begin{pmatrix} 9.8 \\ 6.8 \end{pmatrix} fW \quad \sim \text{small difference with his sheet due to 3}^{\text{rd}} \text{ order approx in band integration in his calculation.} \quad P_{RJb_{ii+1,0}} = \begin{pmatrix} 84 \\ 175 \end{pmatrix} fW$$

my value corrected with the differences in transmissions  $1.10 \cdot 0.54 \cdot 85 = 50.5$  ~ same as  
 from Desert's Excel sheet and including his EffLP for my  $\lambda$ :  $1.15 \cdot 0.42 \cdot 173 = 83.6$  his sheet

Desert included the beam efficiency (EffLP) as a "pixel efficiency" for extended sources, but the convolution of diffraction beam with the source shape says that if the source image is bigger than the diffraction pattern, the illumination is mostly uniform, so  $F_{\text{eff}}$  must be used, not  $B_{\text{eff}}$  !

Point source:  $F_t := 1 \text{ mJy}$

Using the same method as Desert's sheet:

$$P_{\text{ptD}_{ii}} := \frac{\text{EffLP}_{ii}}{5} \cdot \text{tsky}_{D_{ii}} \cdot A \cdot F_t \cdot \delta v_{D_{ii}}$$

$$P_{\text{ptD}} = \left( \frac{0.31}{0.21} \right) 10^{-17} \text{ W} \quad \sim \text{same as his sheet}$$

The factor EffLP/5 comes from the argument that 1/5 of the power is in the pixel, which is compatible with :

$$P_{\text{ptme}_{ii,v}} := \frac{\eta_{\text{pixme}_{ii}}}{F_{\text{eff}_{ii+1}}} \cdot \text{tsky}_{\text{me}_{ii,v}} \cdot A \cdot F_t \cdot 2 \cdot w_{ii+1}$$

$$P_{\text{ptme}} = \left( \frac{1.7}{2.5} \frac{1.4}{1.4} \right) 10^{-17} \text{ W}$$

Values from Ill.2. @ 1mmwv:  $P_{\text{ptob}_{ii+1,0}} = \left( \frac{1.7}{2.5} \right) 10^{-17} \text{ W}$

$$\frac{\eta_{\text{Beffme}_{ii}}}{\eta_{\text{pixme}_{ii}}} = \left( \frac{4.7}{4.7} \right) \Rightarrow \text{Desert's method suggests that EffLP is the (full) beam efficiency, which is apparently confirmed by his "best case" values for EffLP.}$$

**==> Apart the problem of EffLP ( $B_{\text{eff}}$ ) in Desert's calculation for the 1KRJ extended source, and the very bad filters of his "initial case", Desert's and my calculations of powers are consistent, with only some minor differences in the transmission factors.**

Photon noise (approximations):

Shot noise (Poissonian):  $\text{NEP}_{\text{TOT}}^2 = \Sigma \text{NEP}^2$

$$\text{NEP}_{\text{pTD}_{ii}} := \sqrt{2 \cdot h \cdot v_{D_{ii}} \cdot P_{\text{TD}_{ii}}}$$

$$\text{NEP}_{\text{pTme}_{ii,v}} := \sqrt{2 \cdot h \cdot v_{ii+1} \cdot P_{\text{Tme}_{ii,v}}}$$

Bunching noise (boson):  $\text{NEP}_{\text{TOT}} = \Sigma \text{NEP}$

Incoherent beam approximation (spacial coherence:  $\Delta \sim \lambda^2 / A \Omega$ ):

$$\text{NEP}_{\text{biTD}_{ii}} := \sqrt{2 \cdot k \cdot \left( \sqrt{T_{aD} \cdot \text{eta}_{D_{ii}} \cdot P_{aD_{ii}}} + \sqrt{T_{tD} \cdot \text{ett}_D \cdot P_{tD_{ii}}} + \sqrt{T_{\text{supD}} \cdot \text{etsup}_D \cdot P_{\text{supD}_{ii}}} \right)}$$

$$\text{NEP}_{\text{biTme}_{ii,v}} := \sqrt{2 \cdot k \cdot \left( \sqrt{T_{\text{atm}} \cdot \text{eta}_{\text{me}_{ii,v}} \cdot P_{\text{ame}_{ii,v}}} + \sqrt{T_{\text{tel}} \cdot \text{ett}_{\text{me}_{ii}} \cdot P_{\text{tme}_{ii}}} + \sqrt{T_{\text{fme}} \cdot \text{etf}_{\text{me}} \cdot P_{\text{fme}_{ii}}} \right)}$$

Coherent beam approximation

( $\Delta \sim 1$ ):

$$\text{NEP}_{\text{bcTD}_{ii}} := \frac{P_{aD_{ii}} + P_{tD_{ii}} + P_{\text{supD}_{ii}}}{\sqrt{\delta v_{D_{ii}}}} \quad \text{NEP}_{\text{bcTme}_{ii,v}} := \frac{P_{\text{ame}_{ii,v}} + P_{\text{tme}_{ii}} + P_{\text{fme}_{ii}}}{\sqrt{2 \cdot w_{ii+1}}}$$

Numerical application:

Convenient noise unit:  $nu = 1 \times 10^{-17} \frac{W}{\sqrt{Hz}}$

$$\sqrt{2 \cdot h \cdot \nu_{D_{ii}} \cdot P_{aD_{ii}}} = \begin{pmatrix} 1.12 \\ 3.05 \end{pmatrix} nu$$

$$\sqrt{2 \cdot h \cdot \nu_{D_{ii}} \cdot P_{tD_{ii}}} = \begin{pmatrix} 1.14 \\ 1.98 \end{pmatrix} nu$$

$$\sqrt{2 \cdot h \cdot \nu_{D_{ii}} \cdot P_{supD_{ii}}} = \begin{pmatrix} 0.80 \\ 1.40 \end{pmatrix} nu$$

$$NEP_{pame_{ii,v}} := \sqrt{2 \cdot h \cdot \nu_{ii+1} \cdot P_{ame_{ii,v}}}$$

$$NEP_{pame} = \begin{pmatrix} 1.83 & 3.46 \\ 4.44 & 9.08 \end{pmatrix} nu$$

$$\sqrt{2 \cdot h \cdot \nu_{ii+1} \cdot P_{tme_{ii}}} = \begin{pmatrix} 2.40 \\ 4.49 \end{pmatrix} nu$$

$$\sqrt{2 \cdot h \cdot \nu_{ii+1} \cdot P_{fme_{ii}}} = \begin{pmatrix} 1.80 \\ 3.41 \end{pmatrix} nu$$

Desert's sheet (index 1 is for poisson, 2 is for boson):

My exact calculs from III.4.:

$$NEP_{aD1} := \begin{pmatrix} 1.22 \\ 3.22 \end{pmatrix} \cdot nu \quad NEP_{tD1} := \begin{pmatrix} 1.15 \\ 2.00 \end{pmatrix} \cdot nu$$

$$NEP_{supD1} := \begin{pmatrix} 1.44 \\ 2.51 \end{pmatrix} \cdot nu$$

$$NEP_{pam_{ii,v}} := NEP_{pab_{ii+1,v}} \quad NEP_{pam} = \begin{pmatrix} 1.8 & 3.5 \\ 4.6 & 9.3 \end{pmatrix} nu$$

$$NEP_{ptb_{ii+1}} = \begin{pmatrix} 2.4 \\ 4.5 \end{pmatrix} nu \quad NEP_{p77b_{ii+1}} = \begin{pmatrix} 1.8 \\ 3.3 \end{pmatrix} nu$$

=> In the bandwidth integration, the approximation of the spectral power by its value at band center gives correct results (errors are only few %).

NEP<sub>a</sub>: difference due to opacity model (see P)

NEP<sub>t</sub>: OK (linear vs 3rd order approximation)

NEP<sub>sup</sub>: Desert's value from my old Excel sheet: with **esup=0.02** (not 0.05) and **without tfilt !**  
=> **not compatible with his P<sub>sup</sub> !** Using esup=0.05 and tfilt=0.15 in his Excel formula => results ~ = calcul above (same difference as telescope case).

$$\frac{P_{aD_{ii}}}{\sqrt{\delta \nu_{D_{ii}}}} = \begin{pmatrix} 0.32 \\ 1.02 \end{pmatrix} nu \quad \sqrt{2 \cdot k \cdot T_{aD} \cdot \eta_{D_{ii}} \cdot P_{aD_{ii}}} = \begin{pmatrix} 0.80 \\ 2.56 \end{pmatrix} nu$$

$$\frac{P_{tD_{ii}}}{\sqrt{\delta \nu_{D_{ii}}}} = \begin{pmatrix} 0.33 \\ 0.43 \end{pmatrix} nu \quad \sqrt{2kT_{tD} \cdot \epsilon_{tD} \cdot P_{tD_{ii}}} = \begin{pmatrix} 0.82 \\ 1.08 \end{pmatrix} nu$$

$$\frac{P_{supD_{ii}}}{\sqrt{\delta \nu_{D_{ii}}}} = \begin{pmatrix} 0.16 \\ 0.22 \end{pmatrix} nu \quad \sqrt{2 \cdot k \cdot \left( \sqrt{T_{supD} \cdot \epsilon_{supD} \cdot P_{supD_{ii}}} \right)} = \begin{pmatrix} 0.41 \\ 0.54 \end{pmatrix} nu$$

$$NEP_{bame_{ii,v}} := \frac{P_{ame_{ii,v}}}{\sqrt{2 \cdot w_{ii+1}}}$$

$$NEP_{bame} = \begin{pmatrix} 0.86 & 3.09 \\ 2.07 & 8.65 \end{pmatrix} nu$$

$$\frac{P_{tme_{ii}}}{\sqrt{2 \cdot w_{ii+1}}} = \begin{pmatrix} 1.49 \\ 2.12 \end{pmatrix} nu$$

$$\frac{P_{fme_{ii}}}{\sqrt{2 \cdot w_{ii+1}}} = \begin{pmatrix} 0.84 \\ 1.22 \end{pmatrix} nu$$

Desert's sheet (index 2 is for boson):

$$NEP_{aD2} := \begin{pmatrix} 0.54 \\ 1.65 \end{pmatrix} \cdot nu \quad NEP_{tD2} := \begin{pmatrix} 0.48 \\ 0.62 \end{pmatrix} \cdot nu$$

$$NEP_{supD2} := \begin{pmatrix} 0.75 \\ 0.98 \end{pmatrix} \cdot nu$$

My exact calculs from III.4.:

$$NEP_{bam_{ii,v}} := NEP_{bab_{ii+1,v}} \quad NEP_{bam} = \begin{pmatrix} 0.8 & 2.7 \\ 1.9 & 7.9 \end{pmatrix} nu$$

a  $\sqrt{2}$  factor is need to find my result:

$$\frac{NEP_{tD2}}{\sqrt{2}} = \begin{pmatrix} 0.34 \\ 0.44 \end{pmatrix} nu$$

$$NEP_{btb_{ii+1}} = \begin{pmatrix} 1.3 \\ 1.9 \end{pmatrix} nu$$

$$NEP_{b77b_{ii+1}} = \begin{pmatrix} 0.7 \\ 1.0 \end{pmatrix} nu$$

Desert's NEP are compatible with the coherent approximation using  $\Delta=1$ , but for a  $\sqrt{2}$  factor ! This comes from my old excel sheet and **supposed** that the incoming **powers were all polarised** (dp=1 => po=2, instead of po=1 for unpolarized beam, see III.2), but from the calculations of P this is not the case ! => the  $\sqrt{2}$  factor in Desert sheet is a mistake !

=>  $NEP_{bme}$  are bigger than exact calculations because the correct spacial coherence for  $0.5F\lambda$  pixels is  $\Delta=0.8$  (not 1 as in the approximation).

Total photon noise:

$$NEP_{pTD} = \begin{pmatrix} 1.8 \\ 3.9 \end{pmatrix} nu$$

$$NEP_{biTD} = \begin{pmatrix} 2.0 \\ 4.2 \end{pmatrix} nu$$

$$NEP_{bcTD} = \begin{pmatrix} 0.8 \\ 1.7 \end{pmatrix} nu$$

$$NEP_{TD} := \sqrt{NEP_{pTD}^2 + NEP_{bcTD}^2}$$

$$NEP_{TD} = \begin{pmatrix} 2.0 \\ 4.2 \end{pmatrix} 10^{-17} \frac{W}{\sqrt{Hz}}$$

$$NEP_{pTme} = \begin{pmatrix} 3.5 & 4.6 \\ 7.2 & 10.7 \end{pmatrix} nu$$

$$NEP_{biTme} = \begin{pmatrix} 7.7 & 13.0 \\ 13.1 & 28.9 \end{pmatrix} nu$$

$$NEP_{bcTme} = \begin{pmatrix} 3.2 & 5.4 \\ 5.4 & 12.0 \end{pmatrix} nu$$

$$NEP_{Tme, ii, v} := \sqrt{(NEP_{pTme, ii, v})^2 + (NEP_{bcTme, ii, v})^2}$$

$$NEP_{Tme} = \begin{pmatrix} 4.7 & 7.1 \\ 9.0 & 16.1 \end{pmatrix} 10^{-17} \frac{W}{\sqrt{Hz}}$$

Desert 10/2008 Excel sheet (4mm wv):

$$P_{tot} \text{ method (shot noise only)} \quad NEP_{pTds} := \begin{pmatrix} 1.9 \\ 4.0 \end{pmatrix} \cdot 10^{-17} \frac{W}{\sqrt{Hz}}$$

Total from each shot noise component:

$$\sqrt{NEP_{aD1}^2 + NEP_{tD1}^2 + NEP_{supD1}^2} = \begin{pmatrix} 2.2 \\ 4.5 \end{pmatrix} nu$$

not =  $NEP_{pTds}$  because of the error in  $NEP_{supD1}$

$$NEP_{Tds} := \begin{pmatrix} 2.8 \\ 5.6 \end{pmatrix} \cdot 10^{-17} \frac{W}{\sqrt{Hz}}$$

=> Desert's  $NEP_{Tds} > NEP_{TD}$  because of the error in  $NEP_{supD1}$  and the  $\sqrt{2}$  factor from polarisation in the bunching noise components (the effect of different fits for atmosphere opacity is much smaller)

My results from III.4.:

$$NEP_{Tm, ii, v} := NEP_{phTb, ii+1, v}$$

$$NEP_{Tm} = \begin{pmatrix} 4.9 & 7.0 \\ 9.5 & 16.1 \end{pmatrix} 10^{-17} \frac{W}{\sqrt{Hz}}$$

=> My results are totally consistent with exact calculations in III.4. and III.5. **The calculations from Desert's 2008 Excel sheet tend to converge toward mine** (compared to his early work with Benoit), **but there's errors in Desert's sheet remnant from my thesis calculations...**

#### Optimal pixel intrinsic noise

Desert imposes the constraint  $NEP_{int} = NEP_T/2$  (as in my thesis). But the comparison  $NEP_{TD}$  vs  $NEP_{Tme}$  show that without an excellent knowledge of the future instrument optical chain transmission, **the safest attitude to make sure the detector intrinsic noise will be negligible compared to the background is to impose  $NEP_{int} = \min(NEP_T)/6$**  (not  $NEP_T/3$  as expected from the value of  $NEP_{Tme}$  only) !

$$\text{NEP}_{\text{Dint}} := \frac{\text{NEP}_{\text{TD}}}{2} \quad \boxed{\text{NEP}_{\text{Dint}} = \begin{pmatrix} 1.0 \\ 2.1 \end{pmatrix} 10^{-17} \frac{\text{W}}{\sqrt{\text{Hz}}}} \quad \boxed{\text{NEP}_{\text{bare}_{ii+1}} = \begin{pmatrix} 0.8 \\ 1.6 \end{pmatrix} 10^{-17} \frac{\text{W}}{\sqrt{\text{Hz}}}}$$

Though obtained with somewhat different hypothesis and reasonings the instrumental noise from Desert's Excel sheet is only a factor 2 above mine, so they are by chance roughly consistent.

#### TOTAL optimal noise

$$\text{NEP}_{\text{D}} := \text{NEP}_{\text{TD}} \sqrt{1 + 0.5^2} \quad \text{NEP}_{\text{me}_{ii,v}} := \sqrt{(\text{NEP}_{\text{Tme}_{ii,v}})^2 + (\text{NEP}_{\text{bare}_{ii+1}})^2}$$

$$\boxed{\text{NEP}_{\text{D}} = \begin{pmatrix} 2.2 \\ 4.7 \end{pmatrix} 10^{-17} \frac{\text{W}}{\sqrt{\text{Hz}}}} \quad \boxed{\text{NEP}_{\text{me}} = \begin{pmatrix} 4.8 & 7.1 \\ 9.1 & 16.1 \end{pmatrix} 10^{-17} \frac{\text{W}}{\sqrt{\text{Hz}}}}$$

Desert 10/2008 Excel sheet (4mm ww):  $\text{NEP}_{\text{ds}} := \begin{pmatrix} 3.2 \\ 6.3 \end{pmatrix} 10^{-17} \frac{\text{W}}{\sqrt{\text{Hz}}}$  results from III.4.: see  $\text{NEP}_{\text{Tme}}$  vs  $\text{NEP}_{\text{Tm}}$

#### Co-addition of pixels

Consistency of physics : the effect of a physical environment on a system does not depend on the way the observer consider this system, in particular either as a whole or made of N subsystems. Thus N coadded pixels must be equivalent to 1 pixel the same size as them.

Only the throughput changes when scaling from a  $0.5F\lambda$  pixel to a  $1F\lambda$ :  $S_{\Omega_{1F\lambda}} = 4 \cdot S_{\Omega_{0.5F\lambda}}$ . Desert assumes NEP is poissonian and varies as  $\sqrt{N}$ , where N is the number of coadded pixels. But the bunching noise  $\text{NEPb} \sim \sqrt{\Delta} \cdot P$ , and in the  $0.5..4F\lambda$  range  $\Delta \sim 1/\sqrt{N}$  so  $\text{NEPb} \sim N^{3/4}$  (see II.3).

Does the fact that NEPb varies with  $N^{3/4}$  mean that pixels are not independent ? Is it the effect of inter pixel correlation and is it equivalent to the covariance matrix in Zmuidzinas ?

number of pixels to coadd:  $\text{Nb} := 4$

$$2 \frac{3}{4} = 1.5$$

$$\text{NEP}_{\text{ND}} := \sqrt{\text{Nb} \cdot (\text{NEP}_{\text{pTD}}^2 + \text{NEP}_{\text{Dint}}^2) + \text{Nb}^{1.5} \cdot \text{NEP}_{\text{bcTD}}^2}$$

$$\text{NEP}_{\text{Nme}_{ii,v}} := \sqrt{\text{Nb} \cdot [(\text{NEP}_{\text{pTme}_{ii,v}})^2 + (\text{NEP}_{\text{bare}_{ii+1}})^2] + \text{Nb}^{1.5} \cdot (\text{NEP}_{\text{bcTme}_{ii,v}})^2}$$

$$\boxed{\text{NEP}_{\text{ND}} = \begin{pmatrix} 4.7 \\ 10.0 \end{pmatrix} 10^{-17} \frac{\text{W}}{\sqrt{\text{Hz}}}} \quad \boxed{\text{NEP}_{\text{Nme}} = \begin{pmatrix} 11.5 & 17.9 \\ 21.2 & 40.2 \end{pmatrix} 10^{-17} \frac{\text{W}}{\sqrt{\text{Hz}}}}$$

Impossible to define a general formula for  $\text{RN} = \text{NEP}_{\text{N}} / \text{NEP}$  because it depends on  $\text{NEP}_{\text{p}} / \text{NEP}_{\text{b}}$ , only particular cases corresponding to the values calculated previously can be calculated:

$$\begin{array}{ll} \text{NEP}_{\text{p}} = 2\text{NEP}_{\text{b}}: & \text{R4}_{\text{D}} := 2.1 \\ \text{RN}_{\text{D}} := \sqrt{\frac{1}{13} \cdot (11 \cdot \text{Nb} + 2 \cdot \text{Nb}^{1.5})} & \text{R16}_{\text{D}} := 4.8 \\ \text{RN}_{\text{D}} \cdot \text{NEP}_{\text{D}} = \begin{pmatrix} 4.7 \\ 10.2 \end{pmatrix}_{\text{nu}} & \end{array}$$

$$\begin{array}{ll} \text{NEP}_{\text{p}} = \text{NEP}_{\text{b}}: & \text{R4}_{\text{me}} := 2.4 \\ \text{RN}_{\text{me}} := \sqrt{\frac{1}{2} \cdot (\text{Nb} + \text{Nb}^{1.5})} & \text{R16}_{\text{me}} := 6.3 \\ \text{RN}_{\text{me}} \cdot \text{NEP}_{\text{me}} = \begin{pmatrix} 11.8 & 17.5 \\ 22.3 & 39.5 \end{pmatrix}_{\text{nu}} & \end{array}$$



From III.4. the NEP calculated for a  $1F\lambda$  pixel (same size as  $4 \times 0.5F\lambda$  pixels) is:

$$NEP_{1F\lambda_{ii,v}} := NEP_{Tb1F\lambda_{ii+1,v}} \quad NEP_{1F\lambda} = \begin{pmatrix} 12.0 & 18.0 \\ 23.0 & 41.0 \end{pmatrix} \mu K$$

=> The calculation of co-addition as a scaling to a bigger pixel is consistent at few %.

Co-addition is useful to check the calculation of NEP is coherent with variation of pixel size, besides it will help defining convenient sensitivity parameters (NET & NEFD) independent pixel.

Remark: my transmission criterias and the blackbody properties of the background components implies that the constraint on the instrumental noise is  $R_{me}/2=1.2$  less demanding for a  $(1F\lambda)^2$  area than expected from "poissonian" scaling of  $0.5F\lambda$  pixels. Hence the bunching noise implies that it is more (less) demanding to build small (big) pixels than expected from shot noise only !

### Noise Equivalent Temperature Density (NET):

$$\mu K := 10^{-6} K$$

1 pixel:

General formula compatible with Desert's formulation:

$$NET := \frac{NEP \cdot T_{RJ}}{\sqrt{2} \cdot P_{RJ}}$$

Replacing  $P_{RJ}$  with its 1<sup>st</sup> order approximation:

$$NET := \frac{NEP \cdot \lambda^2 \cdot p_o}{\sqrt{2} \cdot S\Omega \cdot t_{sky} \cdot 2k \cdot \Delta v}$$

The  $\sqrt{2}$  factor comes from the sampling frequency and is introduced to make the defined quantity proportional to the integration time. This is stressed in the units by the use of  $\sqrt{s}$  instead of  $\sqrt{Hz}$  (in other words  $\sqrt{Hz}$  refers to the quantity before sampling and  $\sqrt{s}$  refers to the recorded data).

$$NET_{D_{ii}} := \frac{NEP_{D_{ii}} \cdot T_{RJt}}{\sqrt{2} \cdot P_{rjD_{ii}}} \quad NET_D = \begin{pmatrix} 797 \\ 1223 \end{pmatrix} \mu K \cdot \sqrt{s}$$

$$NET_{me_{ii,v}} := \frac{NEP_{me_{ii,v}} \cdot T_{RJt}}{\sqrt{2} \cdot P_{rjme_{ii,v}}}$$

$$\text{Desert's sheet:} \quad \frac{NET_{D_{ii}}}{EffLP_{ii}} \cdot \frac{NEP_{ds_{ii}}}{NEP_{D_{ii}}} = \begin{pmatrix} 2321 \\ 6506 \end{pmatrix} \mu K \cdot \sqrt{s} \quad \sim \text{close to his values}$$

$$NET_{me} = \begin{pmatrix} 401 & 742 \\ 373 & 1164 \end{pmatrix} \mu K \cdot \sqrt{s}$$

=> Desert's NET inherit the problems from EffLP in his  $P_{RJ}$  and the wrong  $P_{sud}$  in his NEP. When introducing these "factors" in the calculation, a small difference with the results of his sheet remains, it is due to the 3<sup>rd</sup> order approx he uses for the band integral.

The source temperature is proportional to the brightness = flux/steradians, which is the quantity to measure for extended sources. For this reason the **NET is often used as a parameter of sensitivity to extended sources**. But since its value depends on pixel size, the universality of such parameter can only exist if it is defined for a standarised size: the FWHM beam or full beam are usually used. Desert uses the FWHM beam (4 pixels), like I do.

Nb coadded pixels:

$$NET_{ND_{ii}} := \frac{NEP_{ND_{ii}} \cdot T_{RJt}}{\sqrt{2} \cdot Nb \cdot P_{rjD_{ii}}}$$

$$NET_{ND} = \begin{pmatrix} 425 \\ 648 \end{pmatrix} \mu K \cdot \sqrt{s}$$

$$NET_{Nme_{ii,v}} := \frac{NEP_{Nme_{ii,v}} \cdot T_{RJt}}{\sqrt{2} \cdot Nb \cdot P_{rjme_{ii,v}}}$$

$$NET_{Nme} = \begin{pmatrix} 241 & 466 \\ 217 & 725 \end{pmatrix} \mu K \cdot \sqrt{s}$$

### Scaling for 4 and 16 pixels

$$\begin{array}{ll} \frac{4}{R4_D} = 1.9 & \frac{NET_D}{1.9} = \left( \frac{420}{644} \right) \mu K \cdot \sqrt{s} \\ \frac{16}{R16_D} = 3.3 & \frac{NET_D}{3.3} = \left( \frac{242}{371} \right) \mu K \cdot \sqrt{s} \end{array} \quad \begin{array}{ll} \frac{4}{R4_{me}} = 1.7 & \frac{NET_{me}}{1.7} = \left( \frac{236}{220} \frac{437}{685} \right) \mu K \cdot \sqrt{s} \\ \frac{16}{R16_{me}} = 2.5 & \frac{NET_{me}}{2.5} = \left( \frac{160}{149} \frac{297}{466} \right) \mu K \cdot \sqrt{s} \end{array}$$

Desert's sheet for 4 pixels (FWHM beam):

$$NET_{ds} := \left( \frac{1164}{3322} \right) \cdot \mu K \cdot \sqrt{s}$$

Desert calculates  $NET_{ds} = NET_{1pixds}/2$  as expected for 4 pixels and a poissonian NEP. Though he neglects bunching noise his scaling is close to mine because his hypothesis on pixel size and transmissions give by chance  $4/R4_D = 1.9$ . Hence the problems come again from EffLP in  $P_{rj}$  and  $P_{sup}$  in NEP, indeed:

$$\frac{\sqrt{4} \cdot NEP_{ds,ii} \cdot T_{RJt}}{4 \sqrt{2} \cdot EffLP_{ii} \cdot P_{rjD_{ii}}} = \left( \frac{1160}{3253} \right) \mu K \cdot \sqrt{s} \quad \text{as for 1 pixel: } \frac{NET_{ds,ii}}{NET_{ND,ii}} = \left( \frac{2.7}{5.1} \right)$$

Small difference with his sheet again due to the 3<sup>rd</sup> order approx of the band integral (whereas I use 1<sup>st</sup> order).

Remark: the definition of NET used here is between the "technical" pNET and the "practical" bNET from III.5. Indeed the sampling factor ( $\sqrt{2}$ ) is included here, but not the observing mode ( $\eta_o$ ).

### Noise Equivalent Flux Density (NEFD):

General formula compatible with Desert's formulation

( $F_{pt}$  = flux from a point source,  $P_{bpt}$  = power in the main beam):

$$NEFD := \eta_o \cdot \frac{NEP_b \cdot F_{pt}}{\sqrt{2} \cdot P_{bpt}}$$

The index b (in  $NEP_b$  and  $P_b$ ) refers to the beam and means this definition does not depend on the pixel size.

The factor  $\eta_o$  is the observing mode efficiency; using Desert's notation:

$$\eta_o := \sqrt{\frac{2}{EffMod}}$$

$\eta_o$  allows the definition of a NEFD directly proportional to integration time. It counts for the signal modulation used to suppress background, and introduces 2 terms: (1) the fraction of time actually spent on the source (typically 80% for On-The-Fly observing mode, and 45% for On-Off [Desert]), the remaining being mainly spent on the background reference, (2) the doubling of the background noise introduced with the subtraction. On-Off is often used with horns, but for filled arrays OTF seems better [IRAM bolo meeting 2008, GISMO].

$$\eta_o := \sqrt{\frac{2}{0.8}}$$

$$\eta_o = 1.58$$

1<sup>st</sup> order approximation using quantities calculated previously:

( $\eta_{beam}$  = integral of the diffraction pattern up to the standard size:  $\eta_{HP}$  for the FWHM or  $\eta_{Beff}$  for the full main beam)

$$NEFD := \frac{\eta_o \cdot \mathbf{RN} \cdot NEP \cdot po}{\sqrt{2} \cdot \eta_{beam} \cdot A \cdot tsky \cdot \Delta v}$$

Link to the NET defined above  
using 1<sup>st</sup> order approximation:

$$\text{NEFD} := \eta_o \cdot \text{RN} \cdot \frac{F_{\text{eff}}}{\eta_{\text{beam}}} \cdot \frac{\text{NET} \cdot 2 \cdot k \cdot \Omega_b}{\lambda^2}$$

As previously, the standard size chosen is the beam FWHM ( $1F\lambda$ ), so 4 pixels coadded.

Problem: in his sheet Desert calculate  $P_{\text{ot}}$  for one pixel and for the full main beam. Since the ratio for his scalling is similar to mine, let use also my ratio for the scalling from one pixel to the beam FWHM:

$$\frac{\eta_{\text{HPme}_{ii}}}{\eta_{\text{pixme}_{ii}}} = \left( \frac{3.0}{3.0} \right)$$

$$\text{NEFD}_{D_{ii}} := \frac{\eta_o \cdot \text{NEP}_{ND_{ii}} \cdot F_t}{\sqrt{2} \cdot 3 \cdot P_{\text{pt}D_{ii}}}$$

$$\boxed{\text{NEFD}_D = \left( \frac{5.7}{17.5} \right) \text{mJy} \cdot \sqrt{s}}$$

$$\text{NEFD}_{\text{me}_{ii,v}} := \frac{\eta_o \cdot \text{NEP}_{N\text{me}_{ii,v}} \cdot F_t}{\sqrt{2} \cdot P_{\text{ptme}_{ii,v}}} \cdot \frac{\eta_{\text{pixme}_{ii}}}{\eta_{\text{HPme}_{ii}}}$$

$$\boxed{\text{NEFD}_{\text{me}} = \left( \frac{2.5}{3.2} \frac{4.8}{10.7} \right) \text{mJy} \cdot \sqrt{s}}$$

In his sheet, Desert does several calculations of NEFD:

- 1<sup>st</sup> calculation: he uses the formula with the FWHM beam NET and  $\Omega_b$  (Glh in his notation).

- 2<sup>nd</sup> calculation: he uses the formula with the NEP of one pixel, 1/4<sup>th</sup> of the full beam  $P_{\text{pt}}$  and the inverse of the scalling needed to get the NEP of the FWHM !

The 2<sup>nd</sup> calculation looks wrong, but he finds for both:

$$\text{NEFD}_{\text{ds}} := \left( \frac{6.3}{17.8} \right) \text{mJy} \cdot \sqrt{s}$$

My results from III.5. (for a  $1F\lambda$  pixel = 4 coadded  $0.5F\lambda$  pixels):

$$\text{NEFD}_{\text{m}_{ii,v}} := b\text{NEFD}_{\text{Tb}_{ii+1,v}}$$

$$\text{NEFD}_{\text{m}} = \left( \frac{2.6}{3.5} \frac{4.8}{10.7} \right) \text{mJy} \cdot \sqrt{s}$$

=> My approximate formulas give again results close to the exact calculations from III.5.

Redoing Desert's calculations with his formulas and his values:

$$\text{FWHM throughput in his formula: } \text{Glh} := \frac{4 \cdot S \Omega_D}{A} \quad \text{Glh} = \left( \frac{4.08}{1.33} \right) 10^{-9} \text{sr} \quad \text{as in his sheet}$$

Desert uses On-Off for his "initial case", not OTF. This is not a mistake, just a choice of configuration. For the calculation of  $\text{NEFD}_D$  I prefer keeping OTF for an easier comparison with  $\text{NEFD}_{\text{me}}$ :

$$\eta_D := \sqrt{\frac{2}{0.45}} \quad \eta_D = 2.11$$

$$\eta_D \cdot \text{NET}_{\text{ds}_{ii}} \cdot \frac{2k \text{Glh}_{ii}}{(\lambda_{D_{ii}})^2} = \left( \frac{6.3}{17.9} \right) \text{mJy} \cdot \sqrt{s} \quad \frac{\eta_D \cdot \text{NEP}_{\text{ds}_{ii}} \cdot F_t}{\frac{5 \cdot P_{\text{pt}D_{ii}}}{4}} \cdot \frac{1}{\sqrt{2}} \cdot \frac{1}{\sqrt{4}} = \left( \frac{6.3}{17.5} \right) \text{mJy} \cdot \sqrt{s}$$

=> Same result as Desert's sheet. So I understand his calculations, but disagree with them:

Desert's 2<sup>nd</sup> calculation looks wrong to me because (1)  $P_{1\text{mJy}}$  in Desert sheet =  $5 \cdot P_{\text{otD}}$  = power in the full beam, and  $5 \cdot P_{\text{otD}}/4$  is NOT the power in the beam FWHM, (2)  $\text{NEP}_{\text{ds}}$  is the NEP in one pixel, so  $\text{NEP}_{\text{ds}}/\sqrt{4}$ , is the NEP in a surface smaller than a pixel ! But by chance  $4/\sqrt{4} = \sqrt{4}$  is the poissonian scalling to get the NEP of the beam FWHM from 1 pixel, and  $5 \cdot P_{\text{otD}}$  is the power in the FWHM if  $\text{EffLP}$  is the efficiency of the beam FWHM ( $\eta_{\text{HP}}$ ), not of the full beam ( $\eta_{\text{Beff}}$ ) as suggested by the formula of  $P_{\text{otD}}$  (hence a ratio 3/5 with my method, see below) ! With this gymnastics both errors cancel each other and the 2<sup>nd</sup> calculation is NEFD for the beam FWHM. Now replacing NET,  $P_{\text{ot}}$  and  $P_{\text{ri}}$  with their parent formulas shows that the 1<sup>st</sup> and 2<sup>nd</sup> calculation are equivalent... but imply that  $\text{EffLP}$  is the pixel efficiency for extended sources in  $P_{\text{rj}}$  !

From previous observations, 4 factors should explain the difference between Desert's result and my calculation using his transmission factors: (1) the scaling from  $P_{pt}$  on one pixel to the power in the beam FWHM is a factor 3, not 5; (2)  $NEP_{ds}$  contains a wrong contribution of  $P_{sub}$  and should be replaced by  $NEP_D$ ; (3) Desert scaling of the NEP from a  $0.5F\lambda$  pixel to FWHM is purely poissonian whereas with bunching it should be  $R4_D$ ; (4) Desert assumes OnOff, not OTF.

$$\text{Thus: } NEFD_{D_{ii}} \cdot \frac{3}{5} \cdot \frac{NEP_{ds_{ii}}}{NEP_{D_{ii}}} \cdot \frac{2}{R4_D} \cdot \frac{\eta_D}{\eta_o} = \left( \frac{6.4}{17.7} \right) mJy \cdot \sqrt{s}$$

=> Same result as the calculations above. So the difference between me and Desert's formula is explained.

In his sheet, Desert does a 3<sup>rd</sup> calculation for the NEFD, using the NET like the 1<sup>st</sup> calculation, but this time it is the NET of one  $0.5F\lambda$  pixel and the corresponding solid angle, and he introduces a scaling factor 1.7 that he calls "*intégrale pondérée optimalement de mesure de flux d'une source ponctuelle par rapport au bruit d'un pixel*". Though this sentence is quite cryptic, it looks like this factor is the right scaling to calculate the power from a point source in the FWHM from the power in the full beam.

Indeed Desert says 1/5<sup>th</sup> of the total power is in the central pixel (see  $P_{pt}$ ) and I showed above that the ratio of the integral of the beam to  $1F\lambda$  versus the integral to  $0.5F\lambda$  is a factor 3:

$$\begin{array}{ll} \text{Thus pixel to Full beam} & \frac{5}{3} = 1.7 \\ \text{vs pixel to FWHM:} & \end{array} \quad \begin{array}{l} \text{including effects of} \\ \text{surface errors I find:} \end{array} \quad \frac{\eta_{Beff_{me_{ii}}}}{\eta_{HP_{me_{ii}}}} = \left( \frac{1.6}{1.6} \right)$$

So if my interpretation of Desert's 1.7 factor is correct the difference between his result and mine should be explained with the following formula (attention! don't forget that downscaling  $NEFD_D$  from 4 to 1 pixels needs a division by  $R4_D$ ):

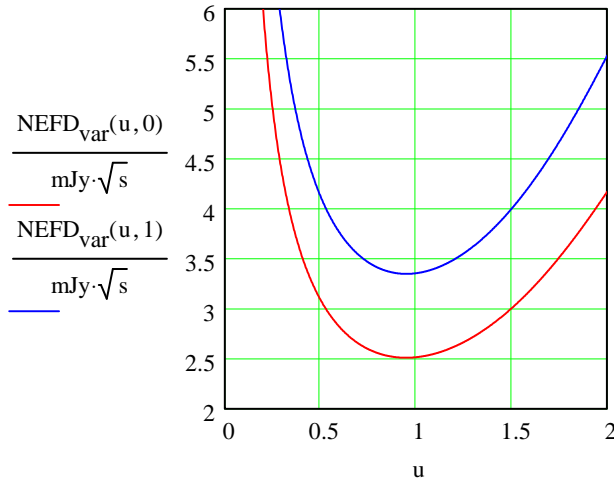
$$\frac{NEFD_{D_{ii}}}{R4_D} \cdot \frac{NEP_{ds_{ii}}}{NEP_{D_{ii}}} \cdot \frac{\eta_D}{\eta_o} = \left( \frac{5.3}{14.8} \right) mJy \cdot \sqrt{s} \quad \text{Which is close to his value: } NEFD_{ds} := \left( \frac{5.3}{15.2} \right) mJy \cdot \sqrt{s}$$

$$\begin{array}{l} \text{Verification redoing the calculation} \\ \text{with his values and formula (attention!} \\ \text{2NET}_{ds} \text{ is the NET for one pixel):} \end{array} \quad 1.7 \cdot \eta_D \cdot \left( 2 \cdot \text{NET}_{ds_{ii}} \right) \cdot \frac{2 \cdot k \cdot S \Omega_{D_{ii}}}{A \cdot (\lambda_{D_{ii}})^2} = \left( \frac{5.3}{15.2} \right) mJy \cdot \sqrt{s}$$

=> From the comparison of Desert's 1<sup>st</sup> and 2<sup>nd</sup> calculations with my calculation of  $NEFD_D$ , the factors (2), (3), and (4) remain. The small additional difference is due to the 3<sup>rd</sup> order approximation of the band integration (see NET). It may seem strange that Desert uses the factor  $1.7 = \eta_{Beff}/\eta_{HP}$  (full beam to half power efficiency) whereas the rest of the formula uses terms calculated for a single pixel ! This oddity is explained remembering that Desert's definition of NET included the  $\text{EffLP} = \eta_{Beff}$  in his calculation of  $Pr_j$ , extracting this factor from his formula, then only remains  $1/\eta_{HP}$  as expected from the theoretical formula linking NEFD to NET shown above. Thus Desert's 1<sup>st</sup> and 3<sup>rd</sup> calculations inherit from the problem of EffLP in NET, itself inherited from the calculation of  $Pr_j$ , but the problem is corrected thanks to the odd scaling factor  $\eta_{Beff}/\eta_{HP}$  !

Now let's go back to my calculation with my transmission parameters and have a look at the evolution of the NEFD with the diameter  $u$  of the disc of integration of the beam ( $u=0.5 \Leftrightarrow 1 \cdot 0.5F\lambda$  pixel,  $u=1 \Leftrightarrow 4 \cdot 0.5F\lambda$  pixels coadded,  $u=2 \Leftrightarrow 16 \cdot 0.5F\lambda$  pixels coadded, etc.). For the optimal atmospheric conditions one gets:

$$\text{NEFD}_{\text{var}}(u, ii) := \frac{\eta_o \cdot \text{NEP}_{\text{me}_{ii},0} \cdot F_t}{\sqrt{2} \cdot P_{\text{ptme}_{ii},0}} \cdot \sqrt{\frac{1}{2} \cdot [(2 \cdot u)^2 + (2 \cdot u)^3]} \cdot \frac{\eta_{\text{pixme}_{ii}}}{\eta_b(u, v_{ii+1})}$$



Verification with the results from III.5. for  $u = 0.5, 1$  and  $2$ :

$$\text{NEFD}_{\text{pm}_{ii},v} := \frac{\eta_o}{\sqrt{2}} \cdot p\text{NEFD}_{\text{Tb}_{ii+1},v}$$

$$u=0.5: \text{NEFD}_{\text{pm}} = \begin{pmatrix} 3.2 & 5.6 \\ 4.4 & 12.7 \end{pmatrix} \text{mJy} \cdot \sqrt{s}$$

$$u=1: \text{NEFD}_{\text{m}} = \begin{pmatrix} 2.6 & 4.8 \\ 3.5 & 10.7 \end{pmatrix} \text{mJy} \cdot \sqrt{s}$$

$$\text{NEFD}_{\text{fbm}_{ii},v} := \frac{\eta_o}{\sqrt{2}} \cdot p\text{NEFD}_{\text{Tb}_{2ii+1},v}$$

$$u=2: \text{NEFD}_{\text{fbm}} = \begin{pmatrix} 3.9 & 7.3 \\ 4.9 & 16.0 \end{pmatrix} \text{mJy} \cdot \sqrt{s}$$

=> This scalable formula of the NEFD is compatible with the exact calculations from III.5. Attention! it is correct only in the same range as the for the approximation  $\Delta \sim 1/u$  in the bunching noise, that is to say in the range  $0.5 < u < 4$  (see III.4.). The behaviour of the curves shows that as expected the optimal point source sensitivity is reached for the beam FWHM, thus the relevance to use this size as the standard size independent from a given pixel size.

Remark: the calculations of the NEFD shown here includes the observing mode factor  $\eta_o$ , whereas the calculations of the NET didn't. I made this choice to be compatible with the approach of Desert's sheet, but it seems incoherent to me: why only one of both sensitivity parameters should includes information on the observing mode ?

## CONCLUSION OF THE COMPARISON BETWEEN F.X.DESERT CALCULATIONS AND MINE FOR THE SPECIFICATIONS OF AN OPTIMAL FILLED ARRAY AT THE 30M TELESCOPE

Though several significative differences exists between Desert's calculations and mine, the estimated optimal performances are consistent in less than an order of magnitude, with point source half power beam width (HPBW or FWHM) optimal sensitivity of few  $\text{mJy} \cdot \sqrt{s}$  for the 1 and 2 mm wavelength bands and On The Fly observing mode. The increase of background due to bad weather degrades this sensitivity by a factor up to 5, but the sky noise inevitably present with bad weather is neglected here while its effect can be much worse. Nevertheless only best observing conditions and maximum dynamics deduced from the power received from strong sources are necessary to define the optimal pixel.

Although Desert's results and mine are more convergent than previous works, some differences between us are still too important to call it compatibility. There's mainly 2 types of disagreements: (1) hypothesis on the physical properties of some elements of the system, and (2) the formulation of some equations. There won't be a final version of this work before the most significative differences recapitulated below are addressed:

- 1) Opacity of the atmosphere: Desert choose a rather mediocre atmosphere, whereas I choose a good atmosphere for the definition of the required optimal pixel noise performances (I also show the effect of bad weather mainly for information, but also to give the goal of the desired dynamics).
- 2) Transmission of the filters: Desert choose rather bad filters ( $t_f=15\%$ ), I choose good filters based on Cardiff's specifications ( $t_f=66\%$  with 7 filters in series). The non-transmitted part of my filters is totally converted in emissivity, whereas part of it could be reflected back to the sky, hence decreasing a bit the NEP and NEFD, so increasing the constraint on the pixel performance, and the difference between Desert and I ! Desert filters are implicitly supposed highly reflective, otherwise their contribution would dominates the background.
- 3) If  $\text{EffLP} = B_{\text{eff}}$  as suggested by its use in most calculations, then its value for the 1mm band is abnormally low. Still, I don't have a final answer on this subject because I haven't fixed yet the problem I discovered comparing  $B_{\text{eff}}$  measurements with heterodyne feedhorns and deductions from antenna tolerance theory and holography measurement of the antenna surface errors.
- 4) Desert uses  $\text{EffLP}=B_{\text{eff}}$  in P1KRJ, whereas I think  $F_{\text{eff}}$  could be used instead.
- 5) Desert doesn't use the same esup and tflt in his calculation of  $P_{\text{sup}}$  than in his calculation of  $\text{NEP}_{\text{sup}}$ , which not calculated from  $P_{\text{sup}}$ , but from a 3<sup>rd</sup> order approximation of the brightness  $B(T_{\text{sup}})$  for a better approximation of the integral in the bandwidth !
- 6) Desert's bunching NEP (boson part) is polarized (introduction of a factor  $\sqrt{2}$ ) whereas that is not the case for the other components.
- 7) Desert's NET inherits the problems from P1KRJ and  $\text{NEP}_{\text{sup}}$ .
- 8) Desert's NEFD 1<sup>st</sup> calculation inherits the same problems as NET, in particular the efficiency hidden in his P1KRJ implies his result is NOT the NEFD for the beam FWHM.
- 9) Desert's NEFD 2<sup>nd</sup> calculation inherit the problem of  $\text{NEP}_{\text{sup}}$  and uses weird scalling ratios for NEP and  $P_{\text{pt}}$  to find a formula equivalent to his 1<sup>st</sup> calculation.
- 10) The results of Desert's 3<sup>rd</sup> calculation is correct in terms of size scalling to get NEFD of the beam FWHM, but this is accomplished thanks to a "pickpocket trick": he applies the scalling factor from full beam efficiency to FWHM efficiency to single pixel quantities, so that the beam efficiency hidden in the P1KRJ of his NET is compensated correctly ! Thus in the end only remains the problem of  $P_{\text{sup}}$  in his result.
- 11) Why including the observing mode factor in NEFD but not in NET ? I think it would be more fair to use the same factors for both sensitivity parameters, isn't it ?

Last important remark: If the pixel efficiency is not included in the definition of the NEFD (as eNEFD in III.5.) this can be highly misleading in terms of sensitivity interpretation (eNEFD keeps decreasing with pixel size). Hence I agree that NEFD should always refers to point source detection and always includes an efficiency term related to the diffraction pattern (so never use eNEFD). I also agree that giving the sensitivity in a unit allowing a direct calculation of the detection time at a standard resolution is very useful for the observer, but such NEFD contains several free parameters that must be specified by the authors: (1) polarization factor, (2) size of the image portion used for the detection compared to the diffraction pattern, and (3) hypothesis on the observing mode. Without these indications, values are always ambiguous and confusing. This remark stands also for the NET...

**All the calculations from this document indicate that compared to MAMBO 2 a factor ~10 improvement in sensitivity could be reached at the 30m telescope.**