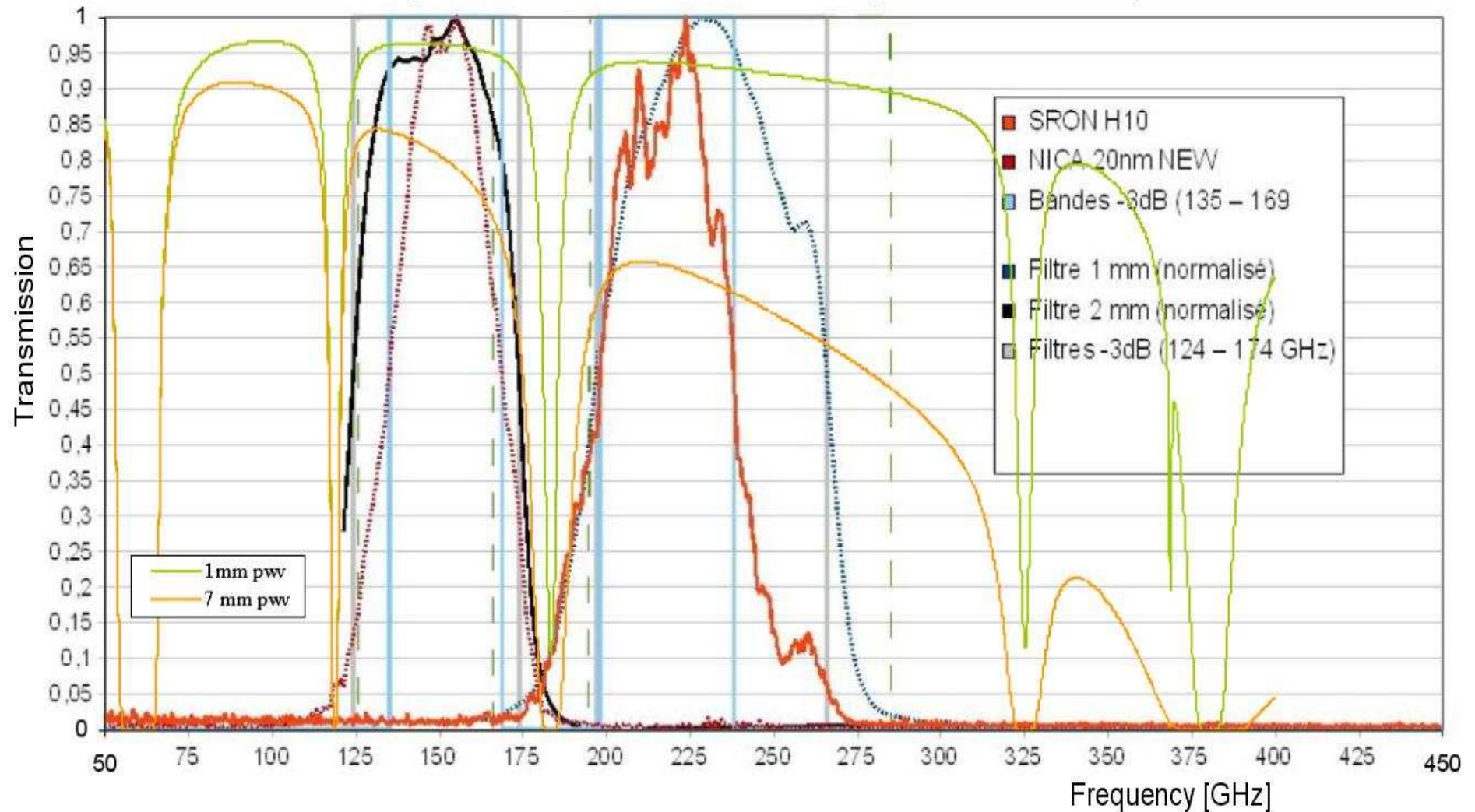


# Extra slides

# New NIKA spectral responses

Transmission profiles: normalized instrument components & PV atmosphere at zenith



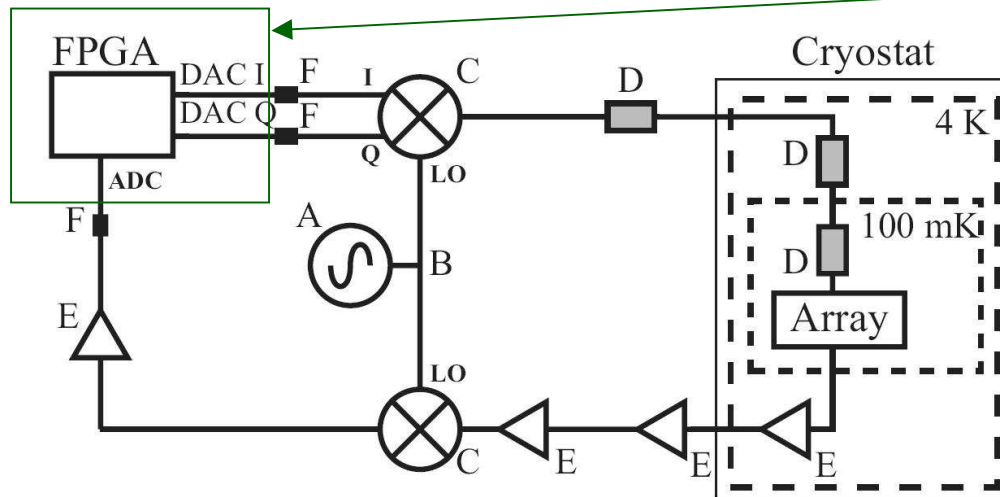
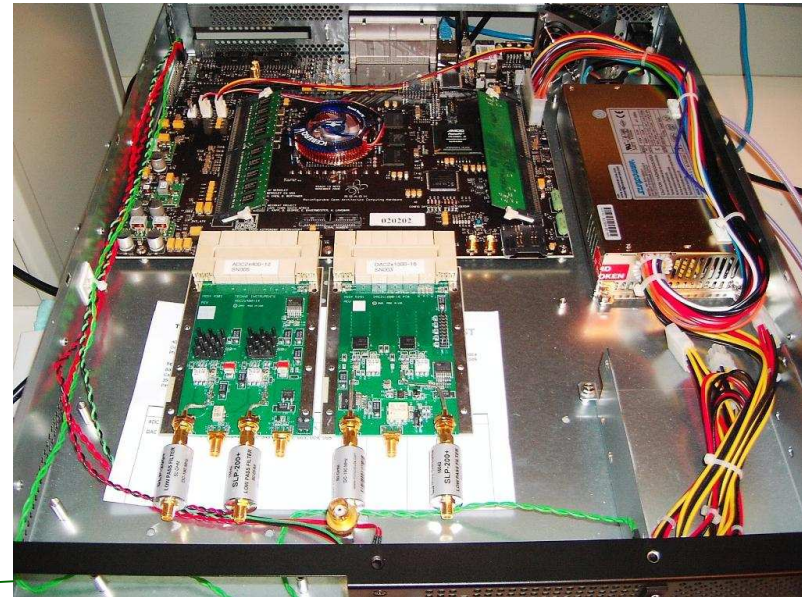
Bands spectral response obtained with a Martin-Puplett interferometer

# New NIKA backend

## Electronics

Based on 2 **CASPER ROACH Boards** from the **Open Source project** (development of 128 channels modules for KIDs readout).

- Rubidium clock reference
- 466 MSPS
- 233 MHz readout
- 72 (1mm band) & 112 (2mm band) "lock-in like" tone generator
- each pixel response broadcasted at 22Hz



A) High frequency synthesizer

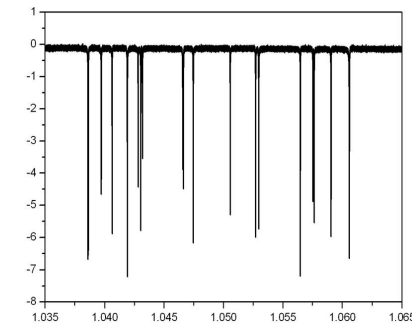
B) Splitter

C) Mixer

D) Attenuator

E) Amplifier

F) Low pass filter

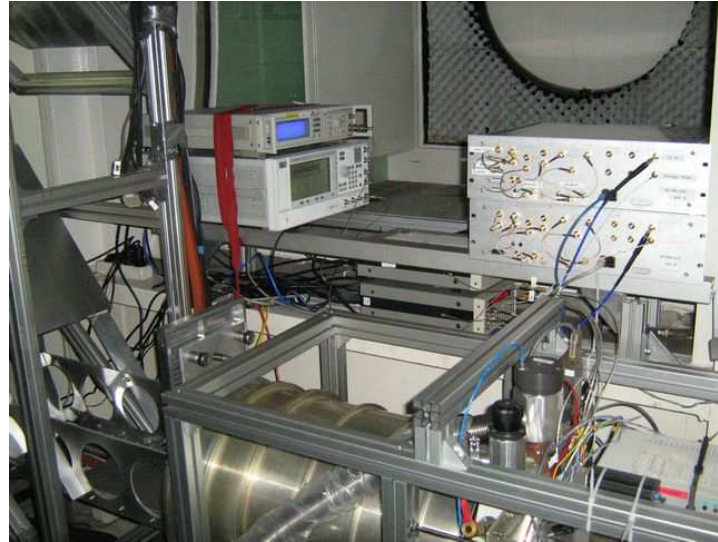


Frequency multiplexing  
1 tone / pixel on a feed line

Individual pixel response = pair of in-phase (I) and quadrature (Q) values.



# NIKA 2<sup>nd</sup> run: Installation in the cabin





# NIKA 2<sup>nd</sup> run: Preparation phase

(acquisition soft, merging with telescope data, detector tuning, ...)

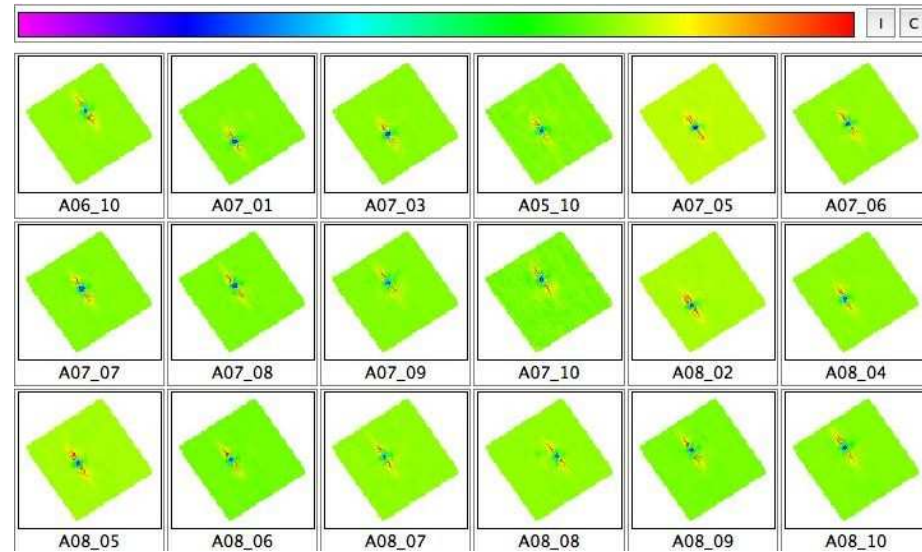


Control room

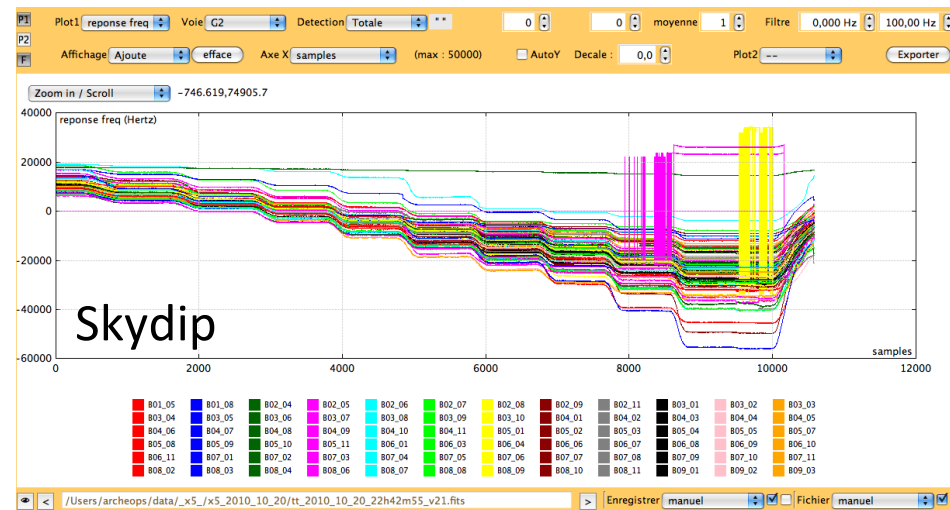


Tuning the resonances

10/05/2011

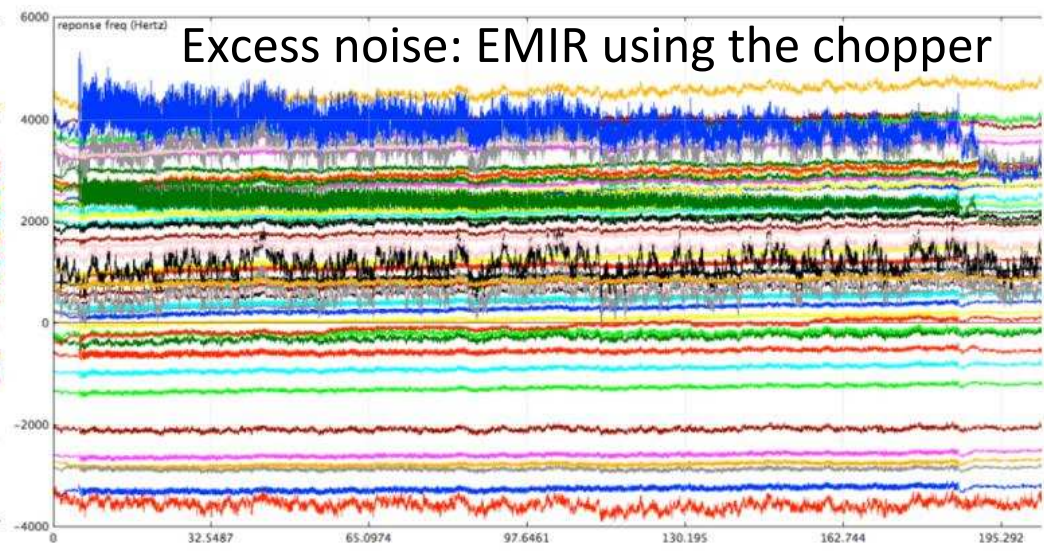
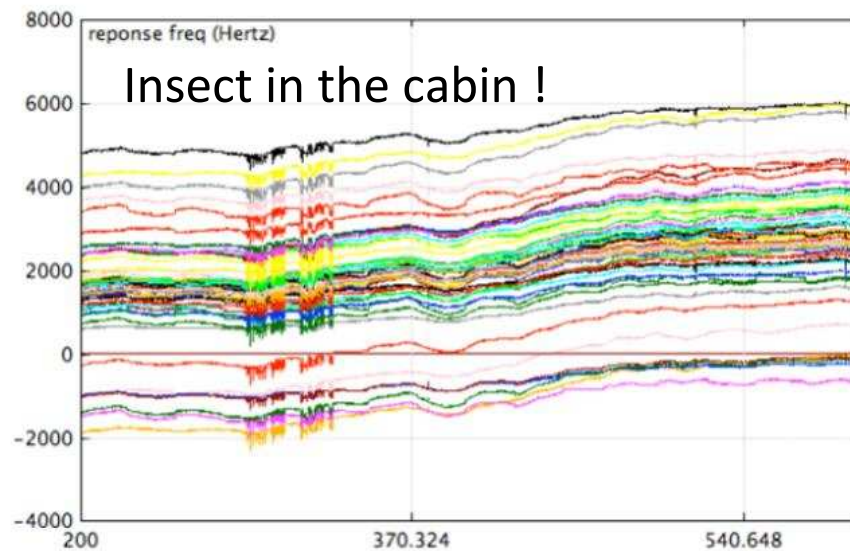
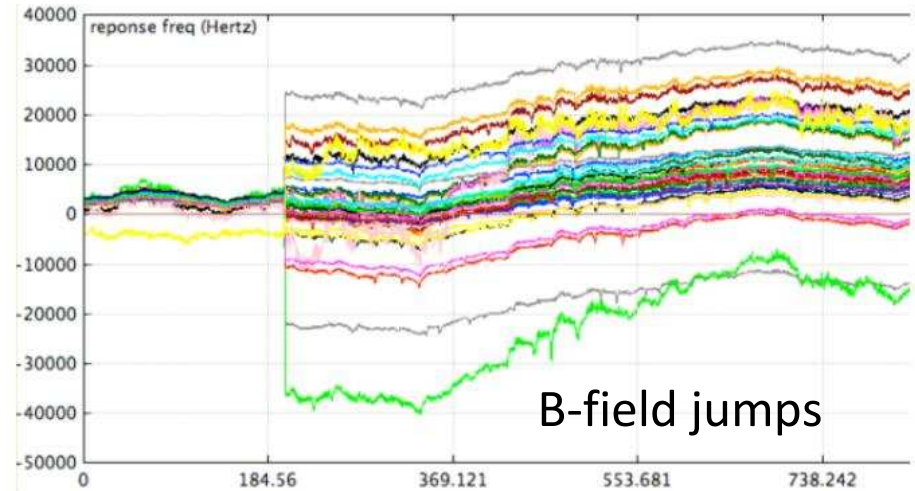


Mars maps (pointing, focus, calibration...)



SAC meeting IRAM Grenoble

# NIKA 2<sup>nd</sup> run: Example of problems





# NIKA 2<sup>nd</sup> run: Data analysis and results

## Calibration

- Only using Response in Frequency signal (better than run1)
- Assumed to be linear with power
- From I and Q, get complex phase on calibration circle, then translate to equivalent frequency shift, as measured during KID tuning

Traditional transmission  
amplitude:

$$A^2 = I^2 + Q^2$$

and phase:

$$\varphi = \text{atan}(Q/I)$$

Equivalent frequency shift:

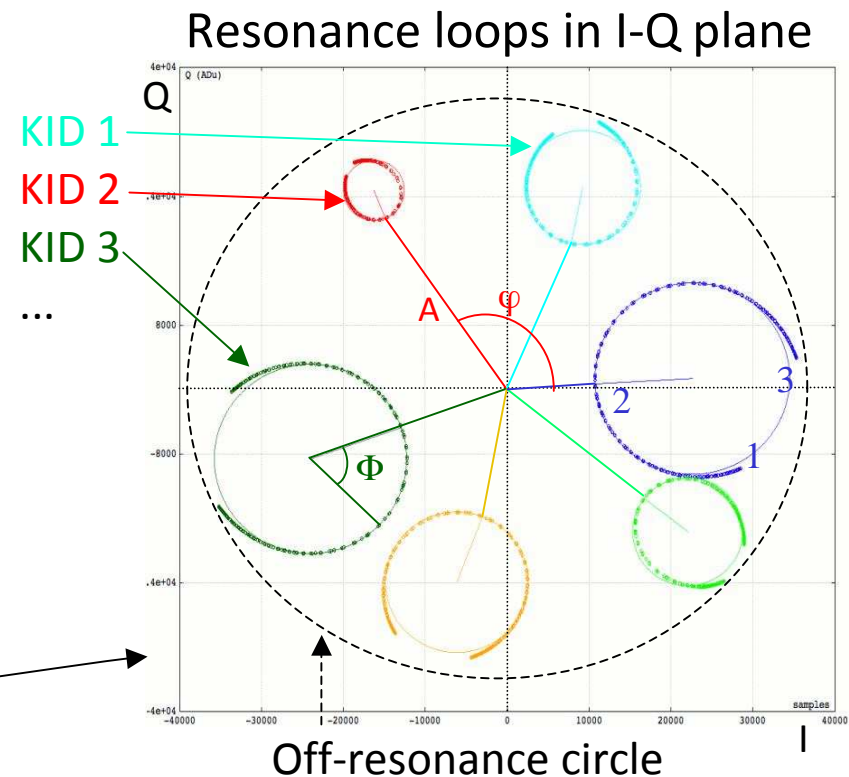
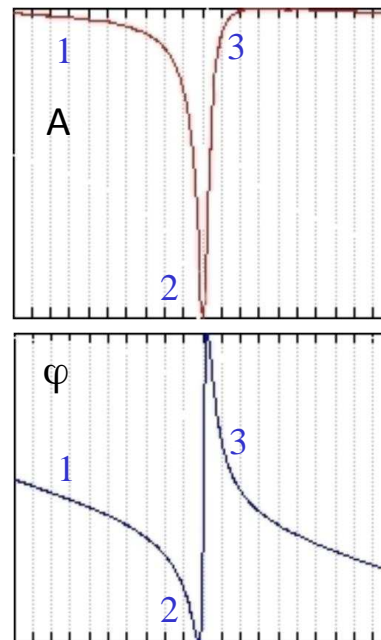
$$\Phi = \text{atan}(Q - Q_c / I - I_c) - \Phi_0$$

$$\sim \delta f_0 \sim (f_0^3 / n_s) \delta P_i$$

$f_0$  = resonance frequency,

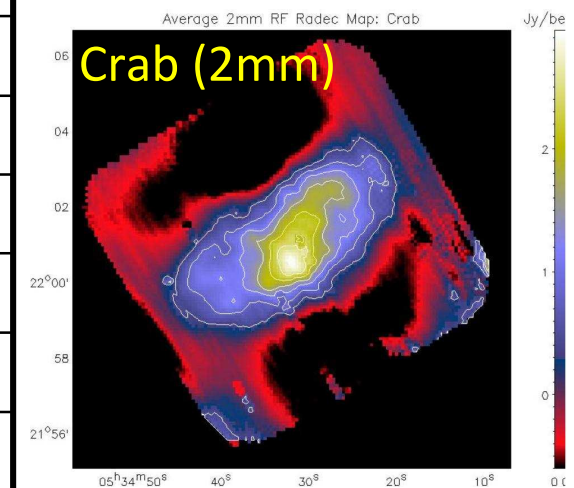
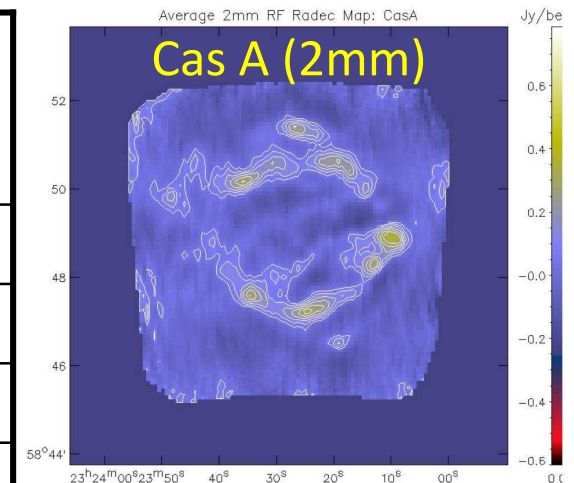
$n_s$  = Cooper pair density,

$P_i$  = incident power



# NIKA 2<sup>nd</sup> run: Data analysis and results

Source	Integration time [s]	Flux measured (1mm , 2mm) [mJy]	NEFD measured (1mm , 2mm) [mJy·s <sup>1/2</sup> ]
Strong sources (no sky decorrelation)			
Neptune	1087	17000 , 7000	2400, 4200
SgrB2(FIR1)	900	76000 , 17700	
MWC 349	495	1700 , 1000	1100 , 1100
IRC 10420	2410	94 , 21	530 , 120
Weak sources (sky decorrelation)			
IRC 10420	2410	94 ± 12 , 21 ± 1	371 , 45
Cyg A	2200	269 ± 34 , 87 ± 22	
NGC 1068	1260	142 ± 25 , 66 ± 3	
PSS 2322	1950	2 ± 12 , 1.1 ± 0.6	330 , 29



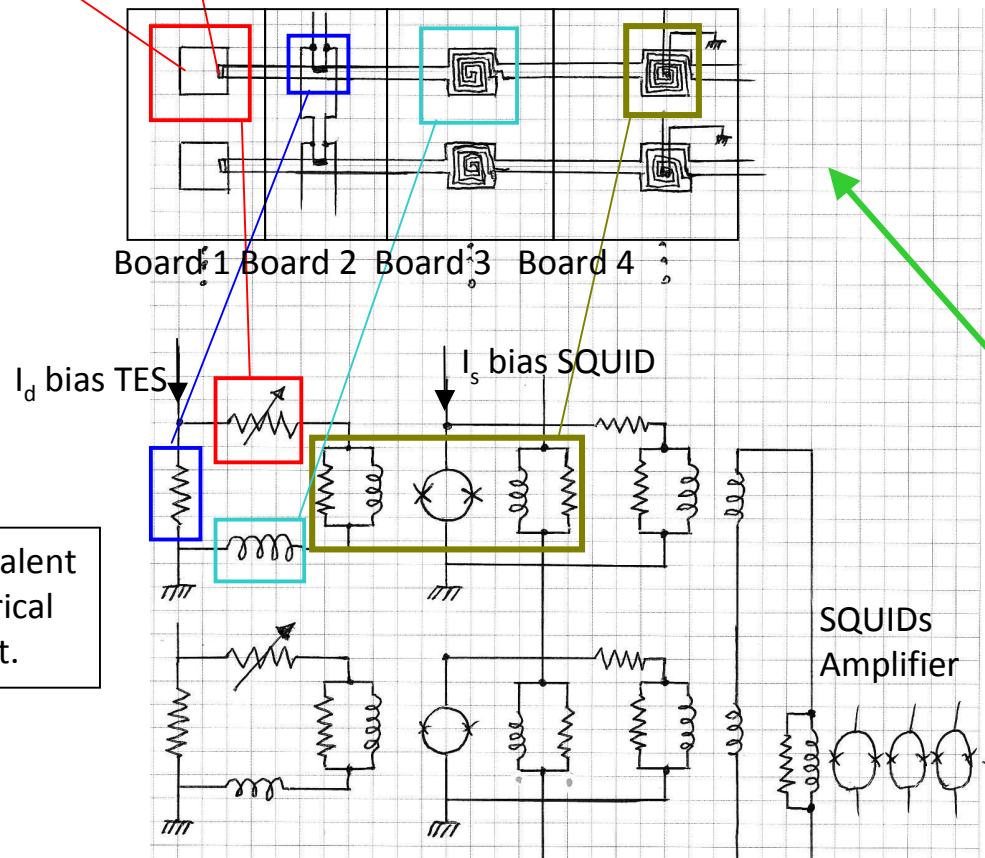
- ⇒ Strong sources: NEFD dominated by source noise (photometric reproducibility)
- ⇒ Weak sources: **conservative NEFDs (mJy·s<sup>1/2</sup>): 400 @ 1mm, 40 @ 2mm**
- ⇒ NET ≈ 4 mK·s<sup>1/2</sup>



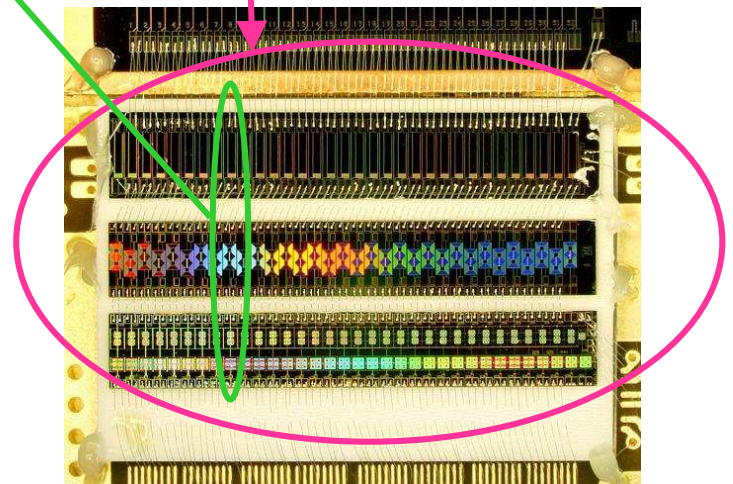
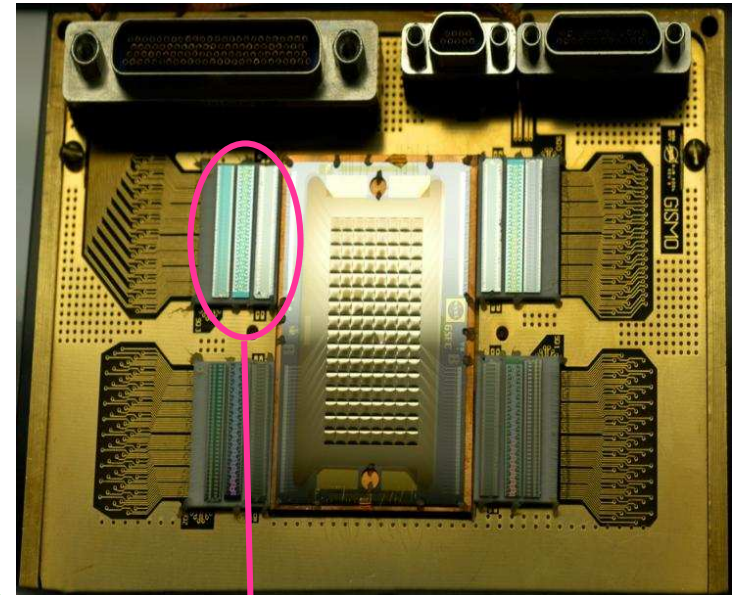
# GISMO backend

Physical aspect of 2 pixels cold backend on a multiplexed line.

Absorber & TES      Bias resistor      Integrator (Nyquist coil)      Multiplexer switch SQUID and its coils



Equivalent electrical circuit.



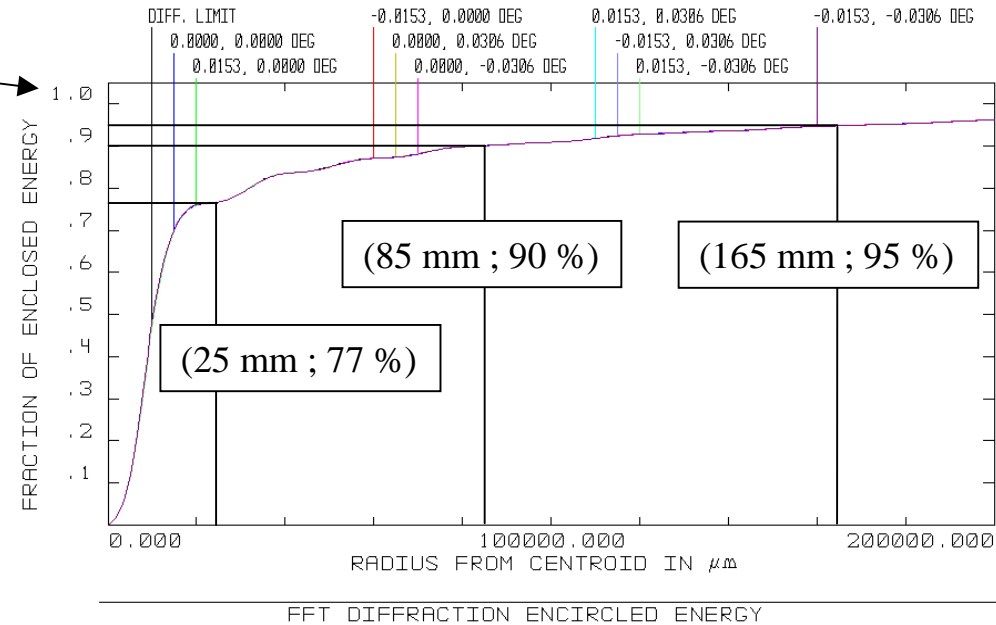
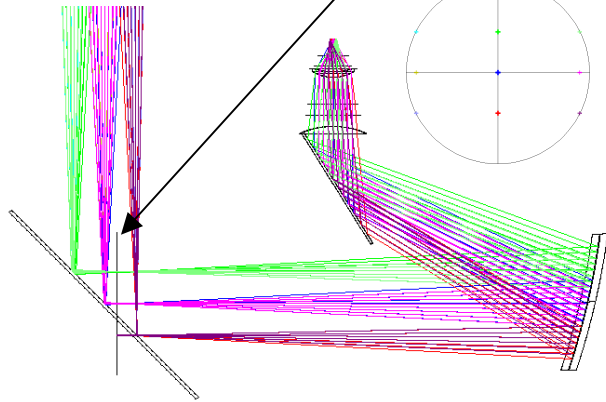


# GISMO 4<sup>th</sup> run: Installation in the cabin



# GSIMO 4<sup>th</sup> run main problem: spill-over on M7

Integrated energy of the diffraction beams at the telescope focal plane

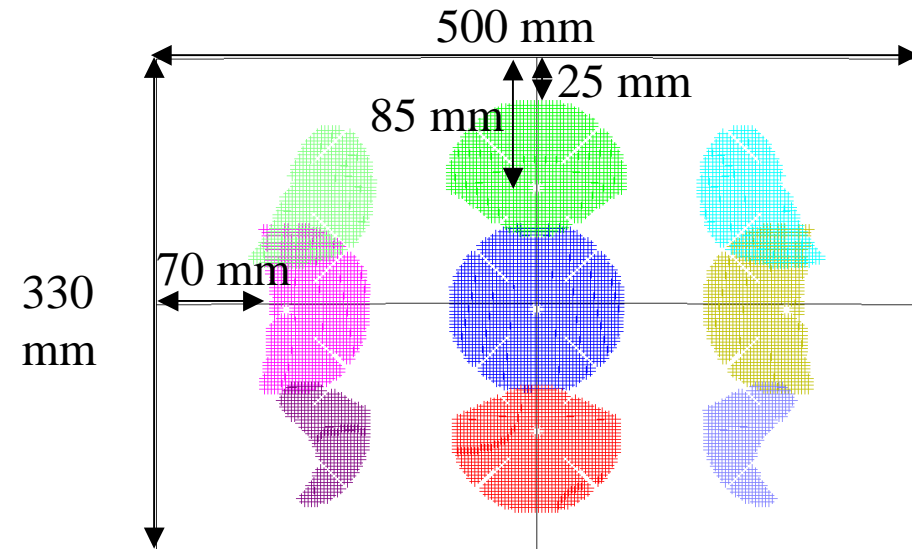


Approximation: each ray PSF has the same shape and FWHM along the optical path as long as it doesn't encounter a powered surface.

=> rays have the same encircled energy diagram anywhere in the cabin, they spill over all the mirrors, M7 being the "worse".

50% of the rays are in the 100 mm radius disc centered on the middle of M7 (~5% spill-over for rays at this position).

=> **global spill-over on M7 ~ 6%.**





# Call: FOV, number of pixels and mapping speed

Number of  $0.5 F\lambda$  pixels filling a given FOV for each atmospheric window available at the 30m telescope:

FOV (diameter)→ Band center ↓	4	6	<b>6.5</b>	7
92 GHz <b>3.25 mm</b>	340	750	880	1020
146 GHz <b>2.05 mm</b>	840	1890	<b>2210</b>	2560
250 GHz <b>1.2 mm</b>	2250	5060	<b>5940</b>	6890
345 GHz <b>0.87 mm</b>	4650	10450	12260	14220

MAMBO-2: 117 pixels, 11" for each pixel HPBW.

Mapping time  $t \sim NEFD^2 \cdot (\Omega_{\text{map}} / \Omega_{\text{e array}}) \Rightarrow$  **mapping speed ratio:**

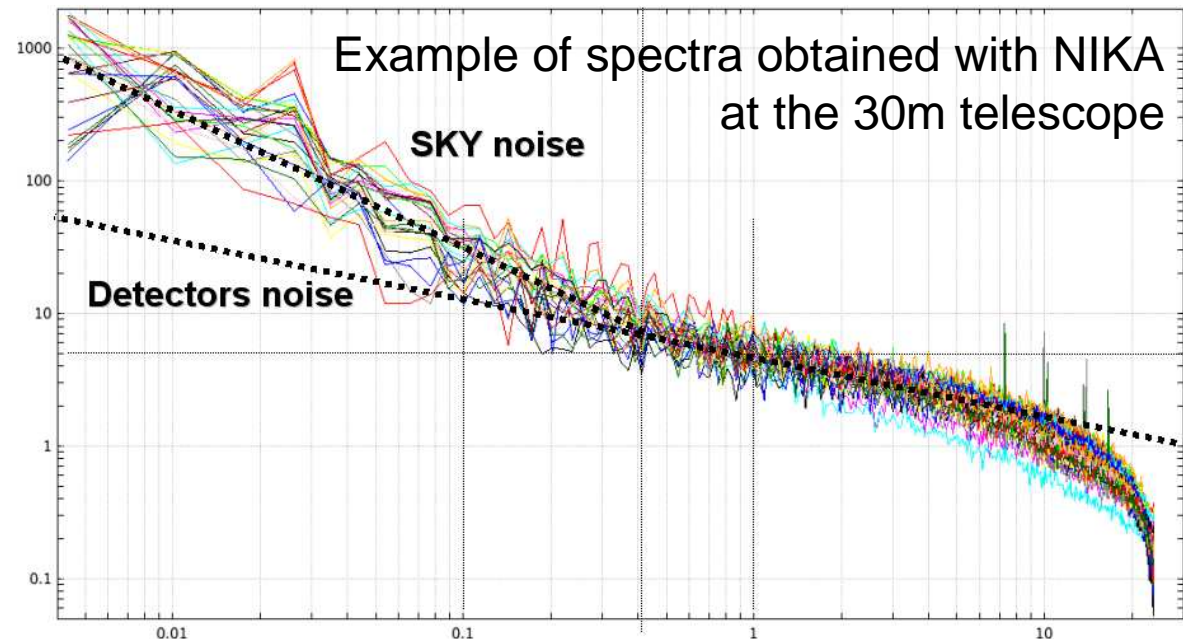
$$t_{\text{MAMBO-2}} / t_{6.5' \text{FOV}, 0.5 F\lambda \text{filled}} = (35^2 / (117 \cdot (11/60)^2)) / (8.6^2 / 6.5^2) \approx \mathbf{180}$$

# Call: Dynamic and frequency range requirements

The background temperature can fluctuate from 20 to 200 K depending on the weather conditions and the elevation. Dynamic range required of an instrument background-limited at any weather condition:  $\Delta T / (\text{NET}/2) = 10^6 \text{ s}^{-1/2}$ .

Typical on-the-fly mapping speed  $\sim 10''/\text{s}$ , typical subscan period  $\sim 10\text{s}$ .

Fluctuations of the atmosphere, and other possible sources (e.g. electronics) create  $1/f$  noise, mostly correlated.



⇒ the **NEP requirements** applies for the **0.1 - 100 Hz** frequency domain

Remark: the pixel to pixel stability should last much longer (several minutes) than the stability of the array

# Call: Calibration, software, operation, budget

## Calibration

The instrument will have to include elements for the calibration of the pixels electrical and optical responses. The specifications for laboratory measurements (e.g. sky simulator) are:

- 5% minimum on the absolute photometry, goal 3%
- 2% minimum on the relative (inter epoch, inter band) photometry, goal 1%.

## Software

A software allowing to control the instrument, do the interface between the instrument and the telescope control system, and provide calibrated data in a defined format should be delivered together with the instrument. As part of the package, the source code of this acquisition software must be available to IRAM and be documented .

## Operation

Cooling of the instrument shall be obtained with a closed cycled cryogenic system with automatic procedures. Maintenance and science operation should be feasible by trained IRAM staff.

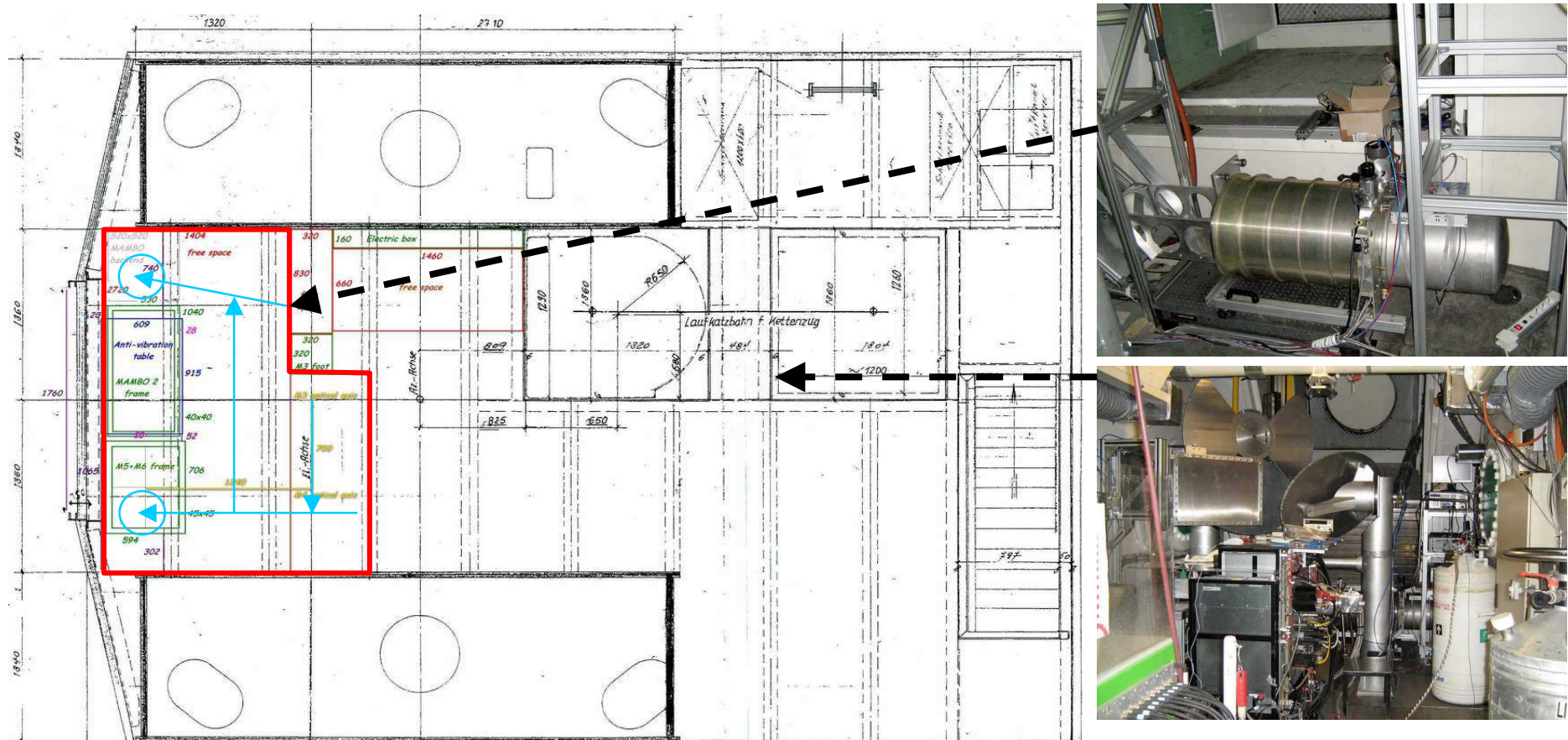
The anticipated instrument lifetime is 10 years.

## Budget

The total budget envelop of the instrument is 2 M€. The proposing consortium will contribute with a budget of 1 M€. This effort will be compensated by guaranteed time for programs using the instrument at the 30m telescope (*~1000 €/h evenly distributed over 4 years, ~125 hours/ semester*).

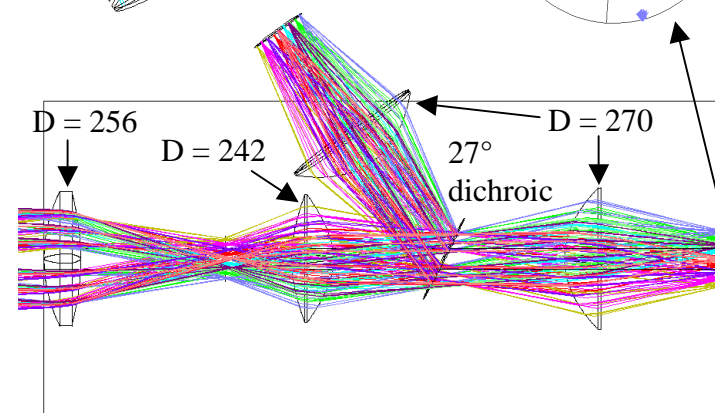
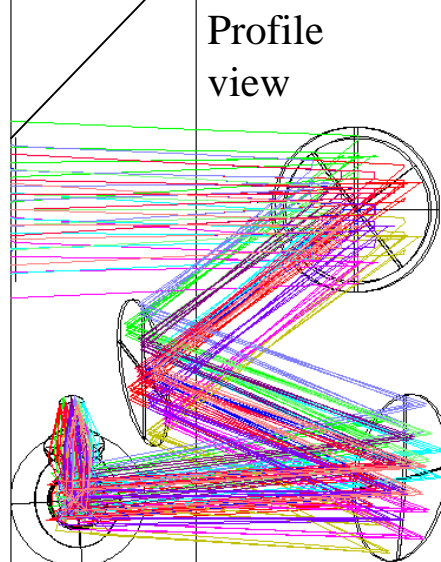
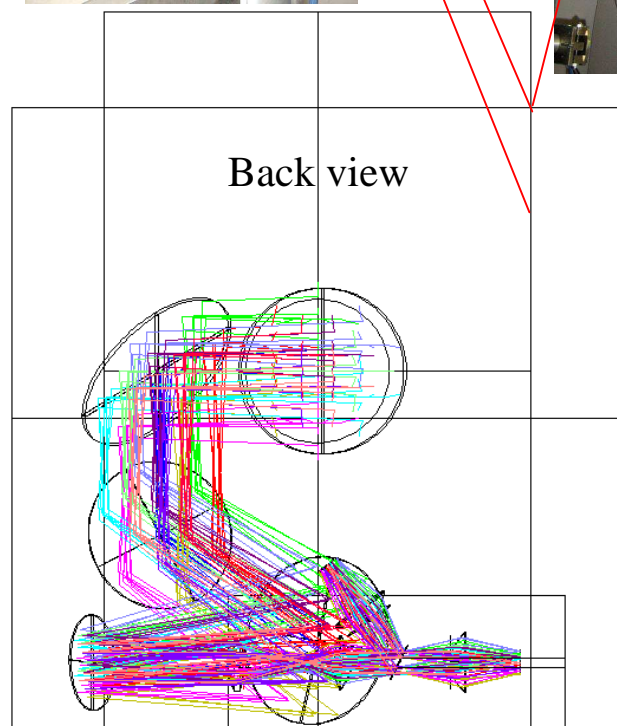
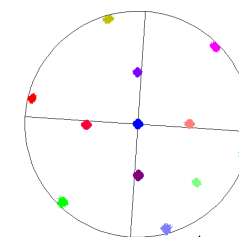
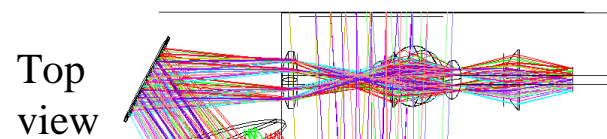
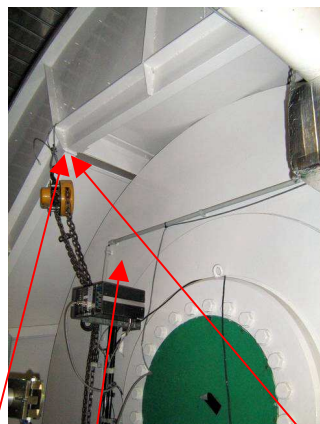
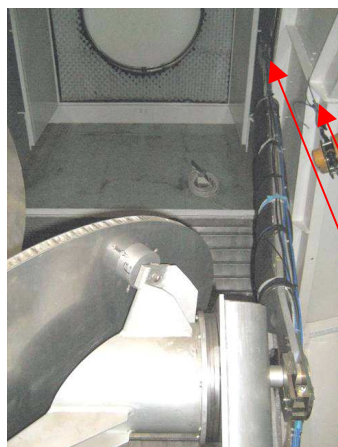


# Call: Room available in the receiver cabin



Space available for the components of the future continuum instrument (red contour), optics and support frame of MAMBO-2 (green), current light path between M3 and M5 (yellow), possible light paths and entries for the future cryostat using a new set of mirrors (light blue arrows and circles). Zemax simulations of the telescope  $\Rightarrow$  FOV limited to 4.5' with current M3, 7' with new M3 (+40% tricking with M2 shift).

# Call: Possible optical design for the future instrument



⇒ The cryostat should not exceed  $0.6 \times 0.6 \times 1.6 \text{ m}^3$ , and the field of view cannot exceed  $6.5^\circ$

# Call: Possible optical design for the future

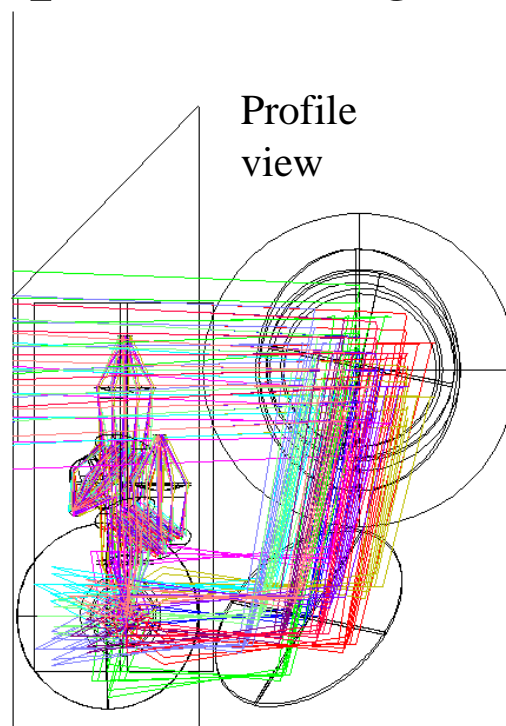
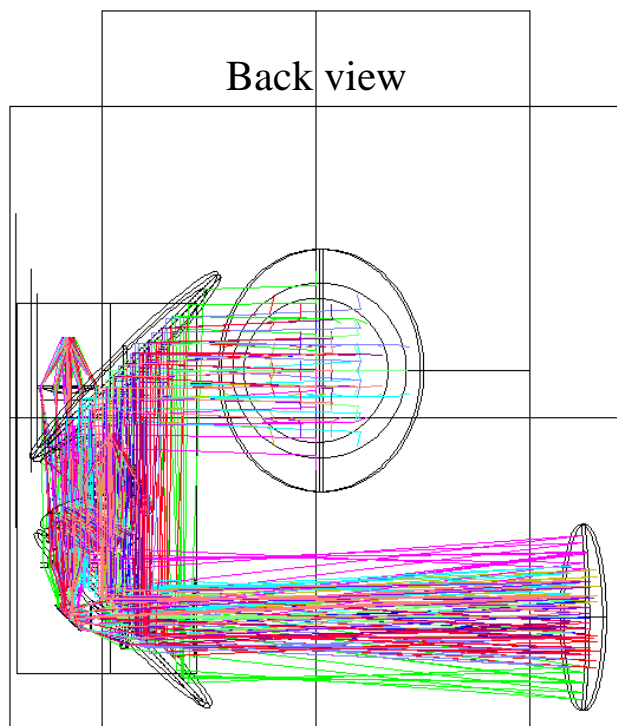
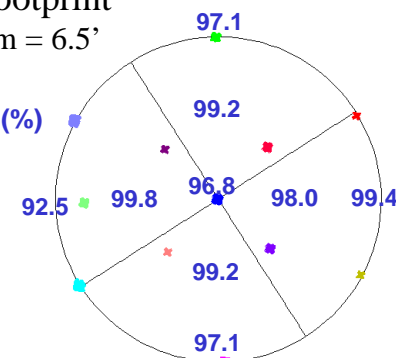
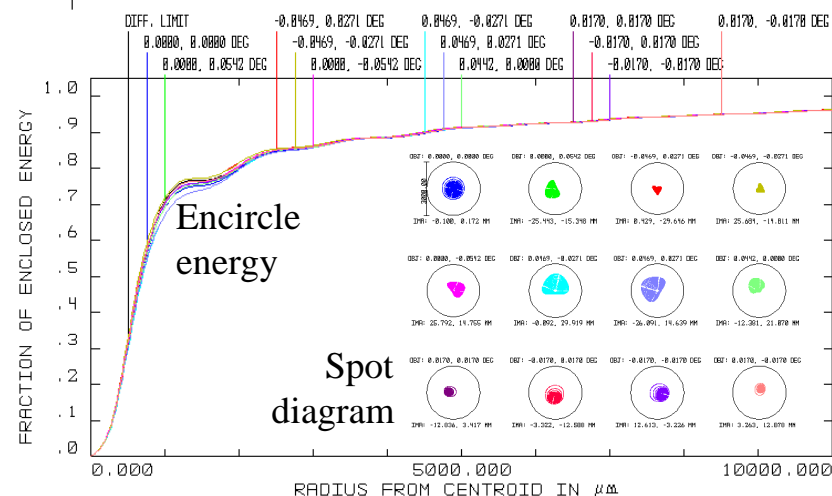
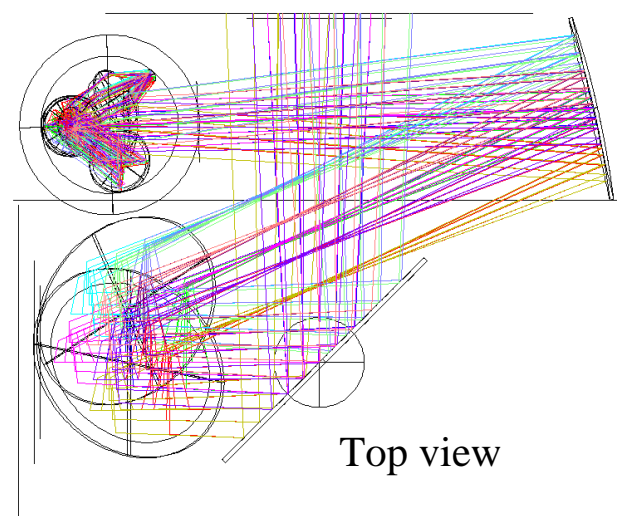
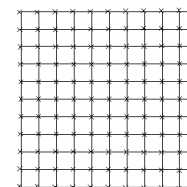


Image footprint  
D = 30mm = 6.5'

Strehl (%)



Grid distortion  
max = 1.5 %





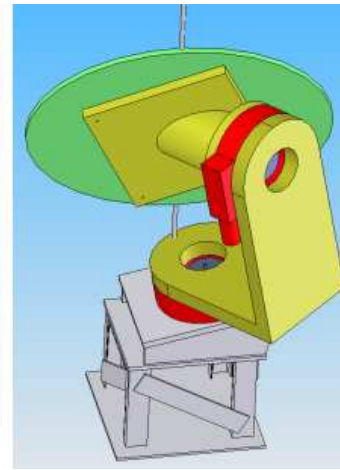
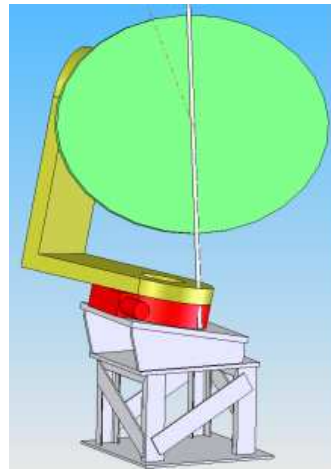
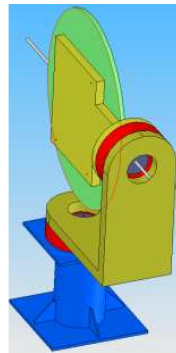
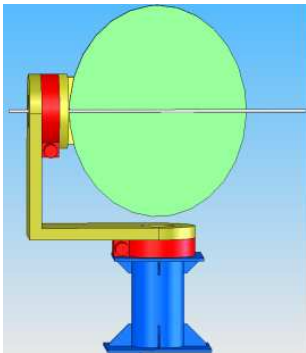
# Call: Increase 30m FOV

## Reorganization of the 30m optics refurbishment project:

- New M3 leg and possibility for motorization
  - New M3 and motorized M4 (Nasmyth ~7' FOV, 2012 ?)
- ⇒ move everything in the cabin + new mirrors after M4.

S2: "tilted pseudo-Nasmyth"

S1: "one-armed alt-azimuthal"



S3: "horizontal az-alt"

